

Inductive Impedance and Saw Tooth Instability

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Workshop on Broadband Impedance
Measurements and Modeling

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- Inductive Impedance
- Wake potentials of short bunches
 - ◆ Bellow
 - ◆ Tapers
 - ◆ Surface roughness wake fields
- Resonator wake fields
- Fokker-Planck Equation
- Longitudinal Instabilities
 - ◆ Microwave instability
 - ◆ Sawtooth instability
- Summary

Inductive Impedance

- Inductive impedance or inductive wake potential are usually used for the description of the wake fields, responsible for the bunch „self-acceleration“, when the „head“ of the bunch loses energy and the „tail“ gets it back. So the full energy loss of the bunch is very small in comparison with the bunch energy spread.
- It usually happens when the bunch is passing by the bellows, tapers, pumping slots, masks, BPMs, or is moving inside resistive or rough vacuum chamber.

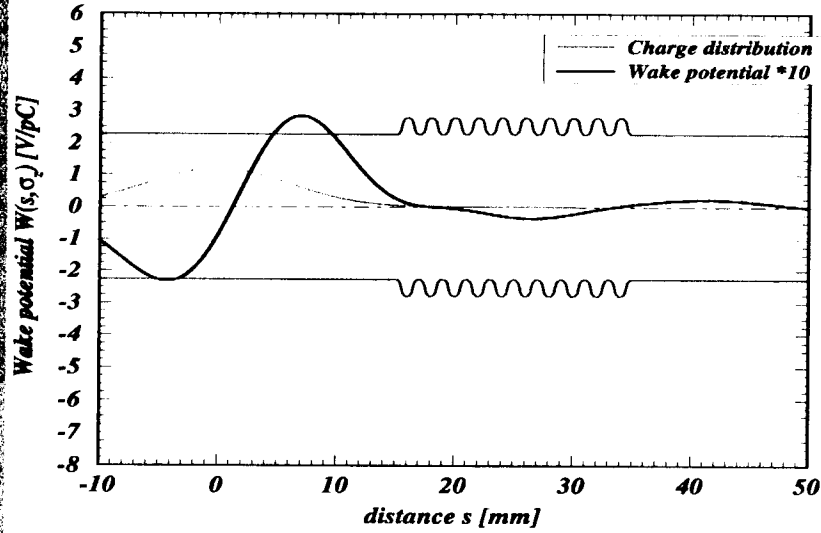
Inductive Impedance

- The inductive impedance sometimes is considered to be the low frequency part of the wake fields.
- More accurate study shows that the „inductive“ structure of the wake potentials is due to the action of the very high frequency fields.
- We present some examples:
 - Bellow
 - Shielded bellow
 - Transition for a quadrupole

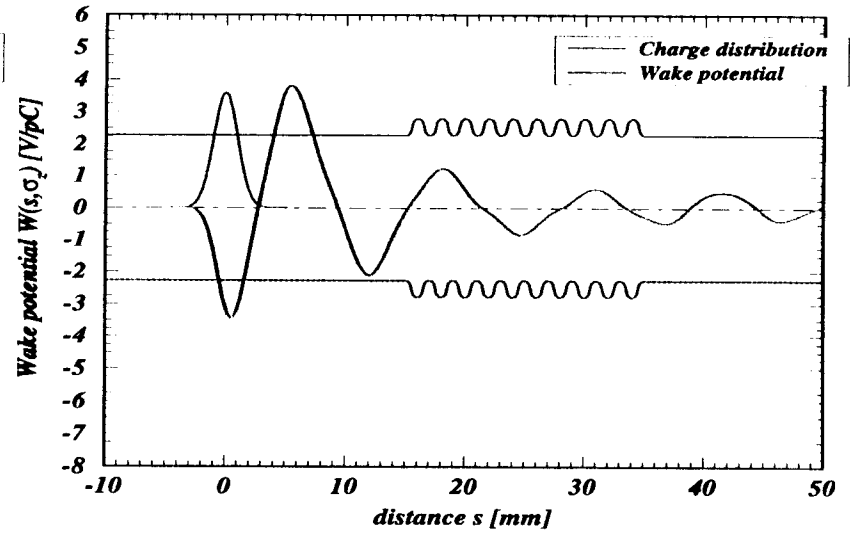
Wake potentials of a bellow

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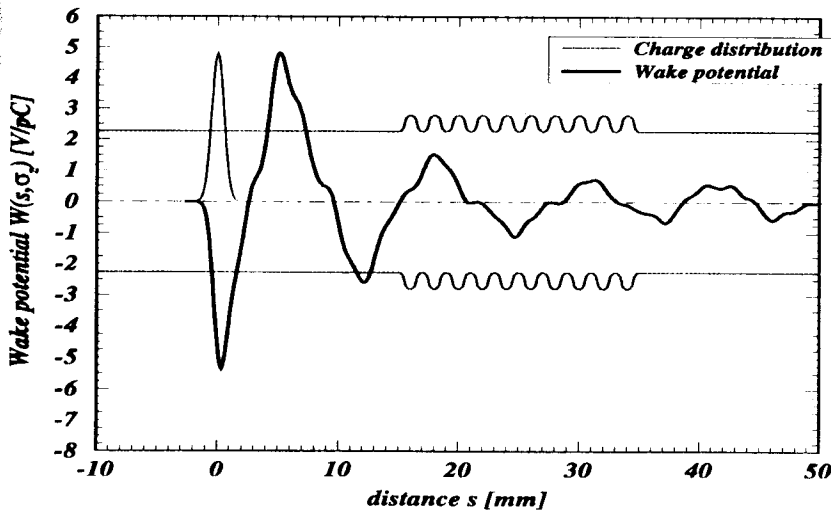
Bunchlength $\sigma_z = 6.0\text{mm}$



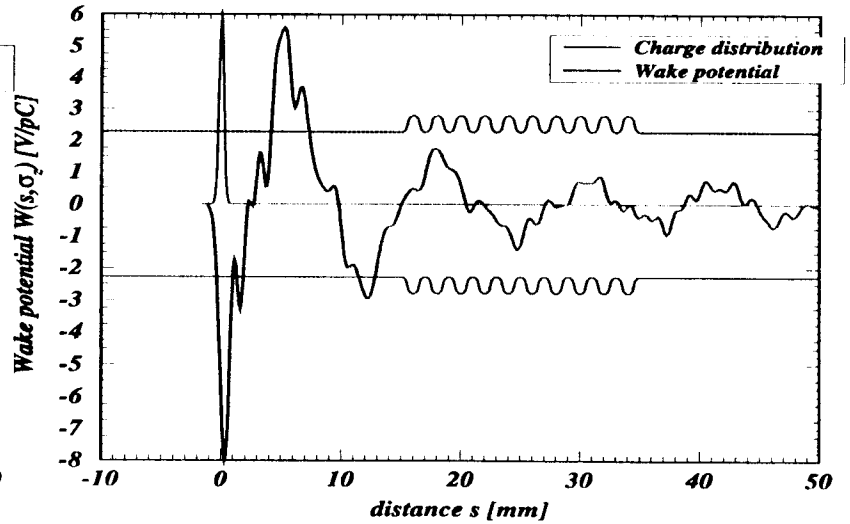
Bunchlength $\sigma_z = 1.0\text{mm}$



Bunchlength $\sigma_z = 0.5\text{mm}$



Bunchlength $\sigma_z = 0.2\text{mm}$



Resonator wake field

- Sometimes these high frequency fields can be fully described by a simple wake function -
- Resonator wake function

$$w(s) = -W_0 \frac{1}{k_Q} \frac{d}{ds} \left[\exp\left(-\frac{k}{2Q}s\right) \sin k_Q s \right]$$

$$k_Q = k \sqrt{1 - \frac{1}{4Q^2}}$$

- Resistive wall wake fields
- Thin dielectric layer inside vacuum chamber
- Surface roughness wake fields and shallow bellows

Inductive Wake Potentials

- The wake potential of the bunch for the high frequency ($k\sigma_z \gg 1$; $Q \gg 1$) wake function is

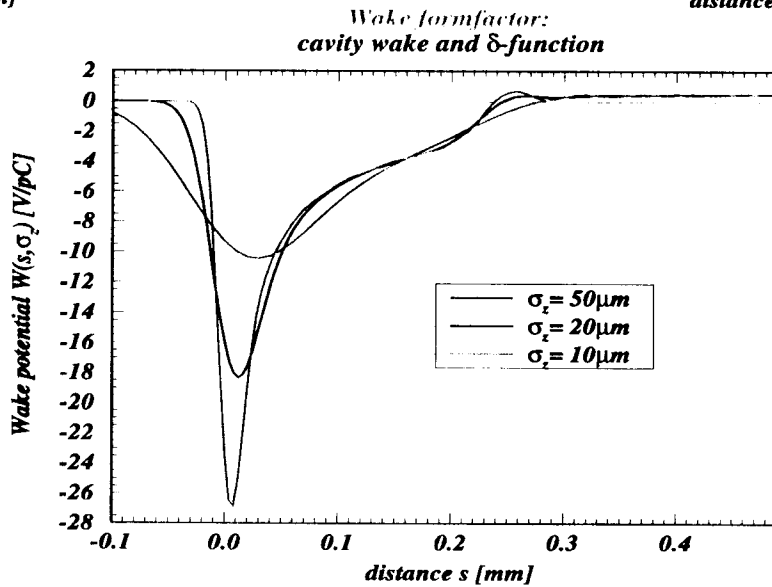
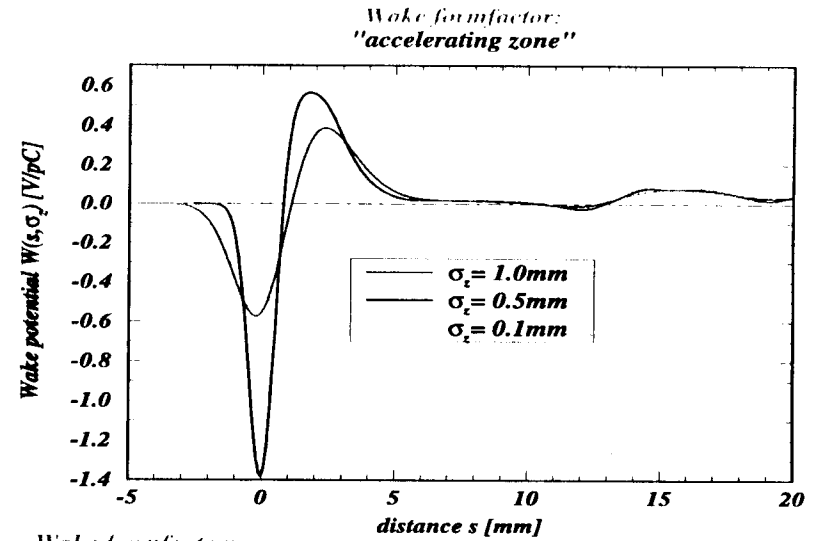
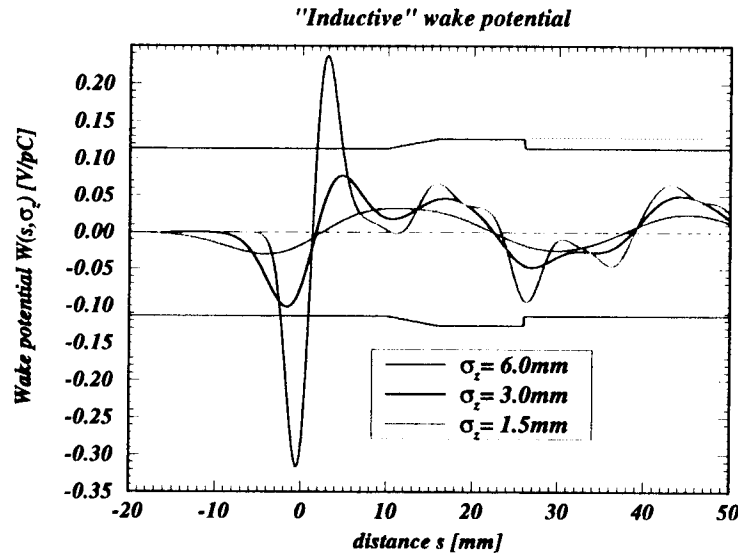
$$W(s) \approx qW_0 \int_{-\infty}^s \rho(s') \cos k(s-s') ds' \approx qW_0 \frac{\pi}{k^2} \frac{\partial}{\partial s} \rho(s)$$

- Loss factor $K_{loss} = \int_{-\infty}^{\infty} \rho(s)W(s)ds = 0$

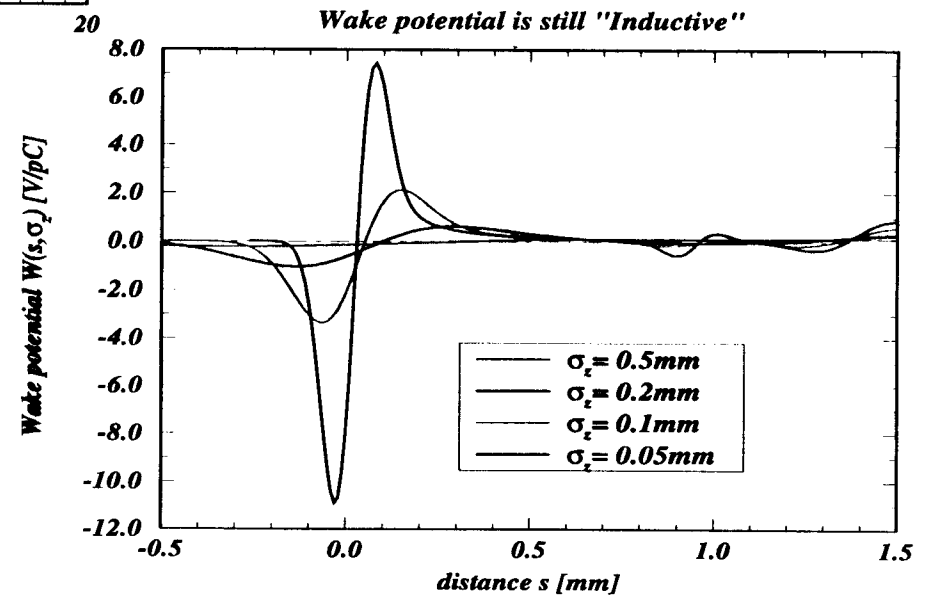
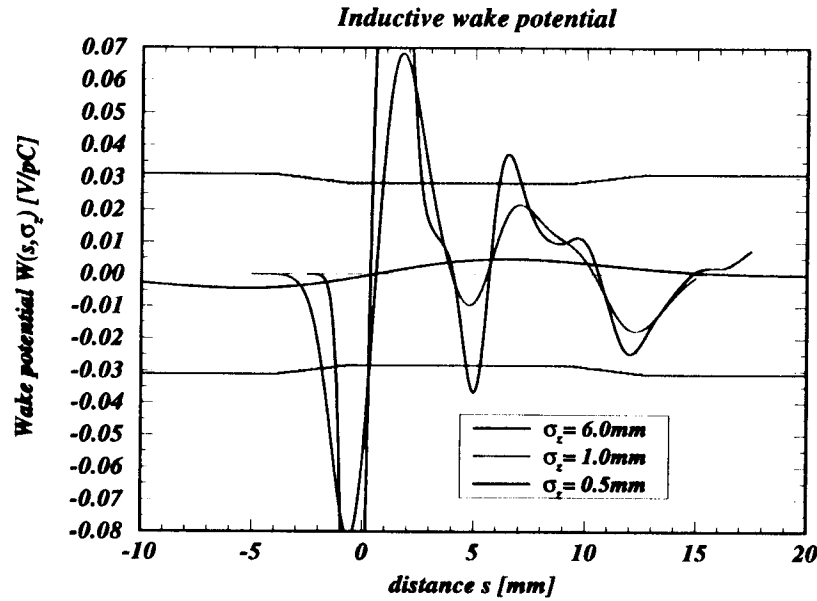
- Energy spread Gaussian bunch

$$\Delta E_{wake} = \sqrt{\int_{-\infty}^{\infty} \rho(s)W^2(s)ds} \quad \Delta E_{wake} = q \frac{W_0}{(k\sigma_z)^2} \left(\frac{\pi}{6\sqrt{3}} \right)^{1/2}$$

Shielded bellow

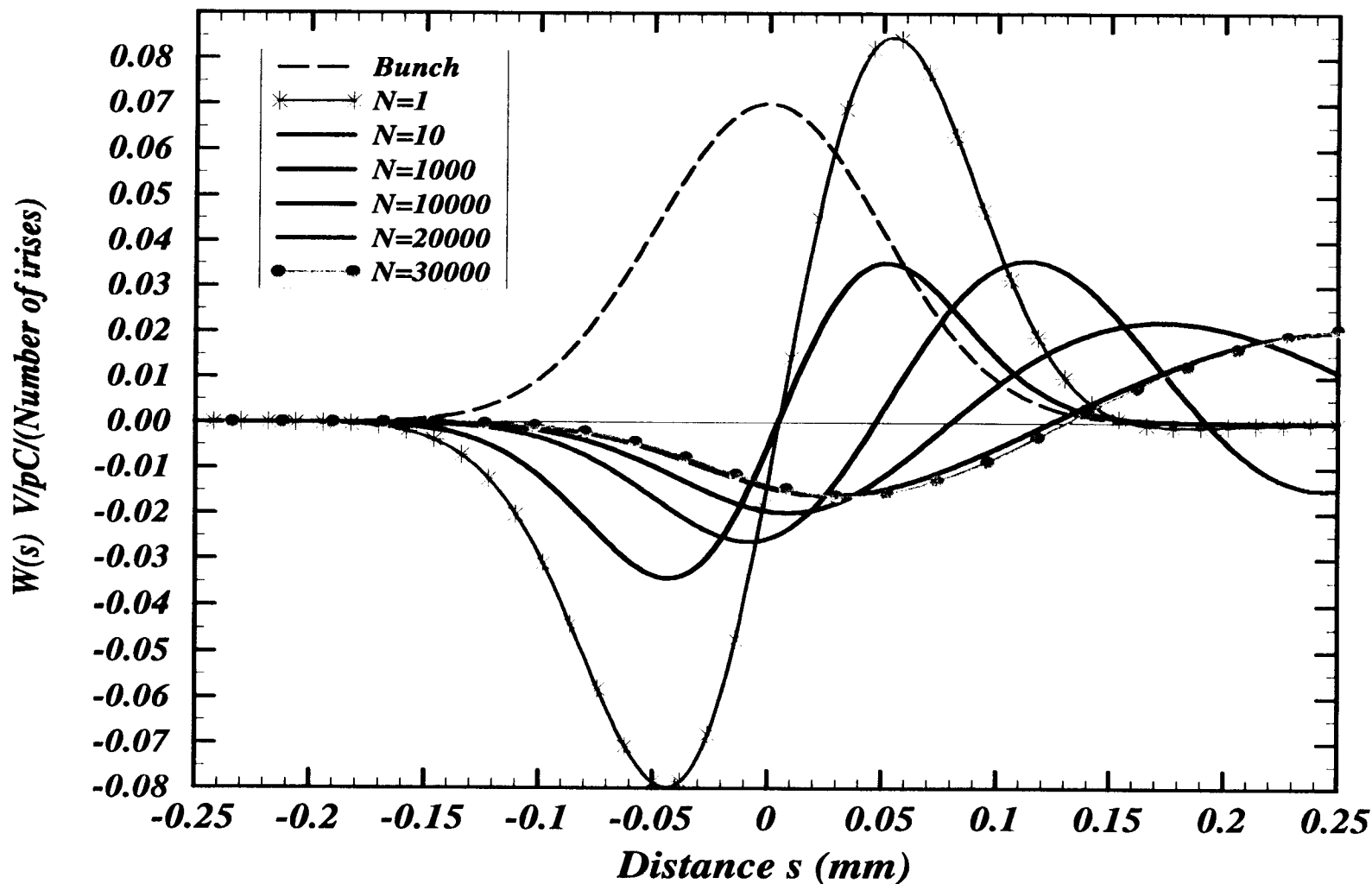


Transition for a quadrupole



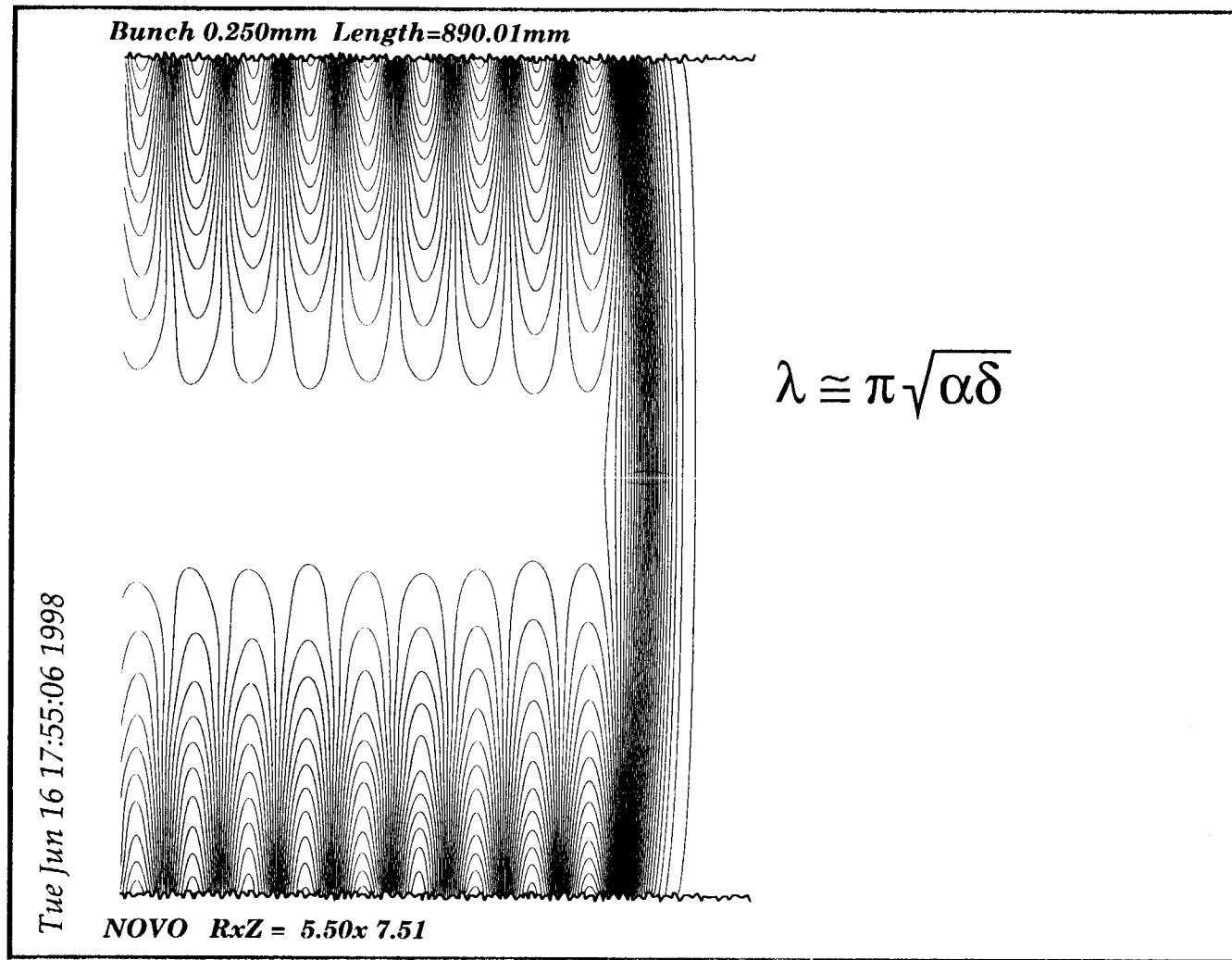
Wake fields in periodic „rough“ surface structure

Bunch of $\sigma=50\mu$ in the tube of $R=5\text{mm}$ with irises of 10μ by 10μ , period is 20μ . $N=1,10,1000,10000,20000,30000$



Surface roughness wake field

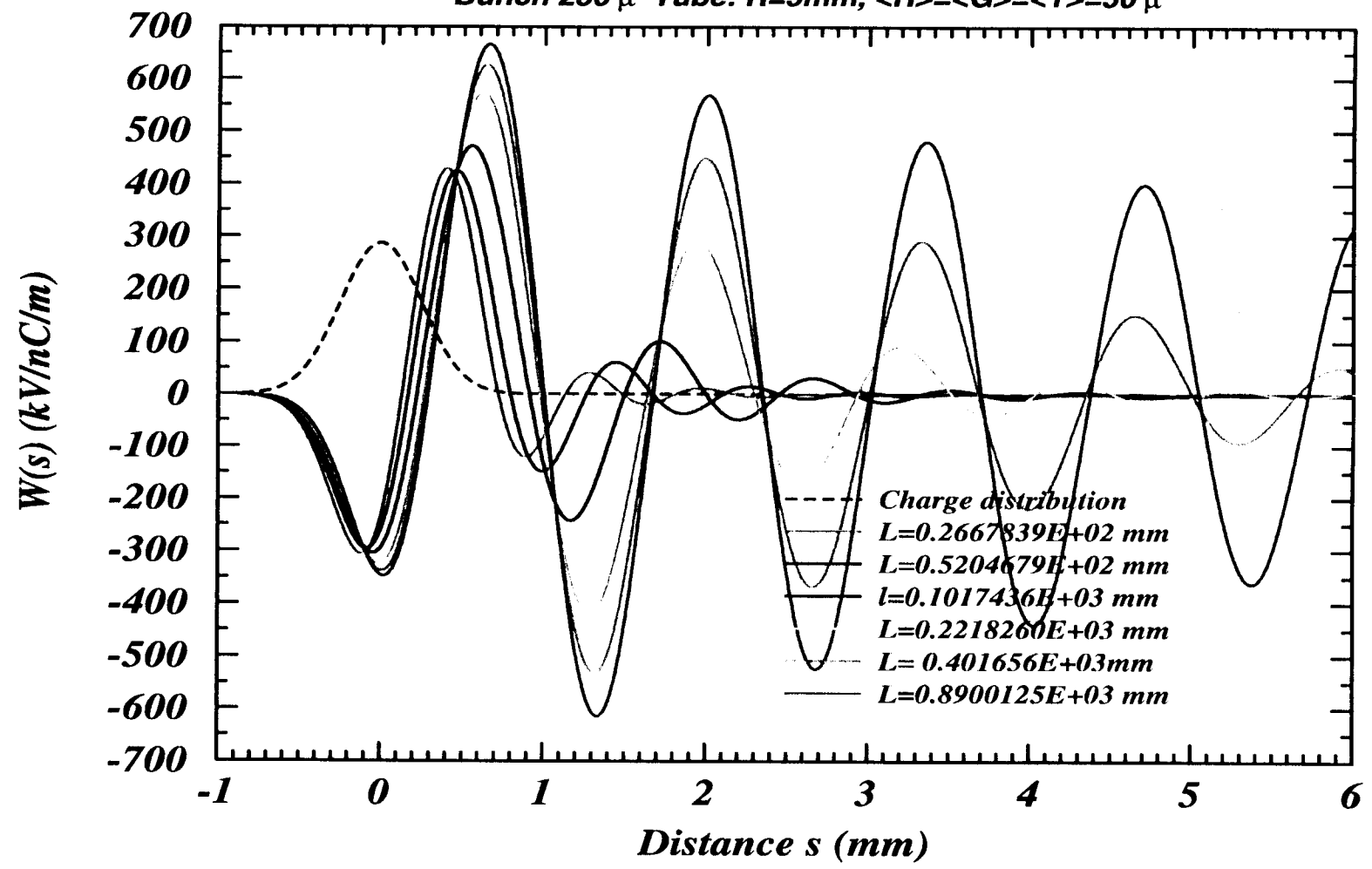
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Surface roughness wake potential

Normalised Wake Potential for different tube length

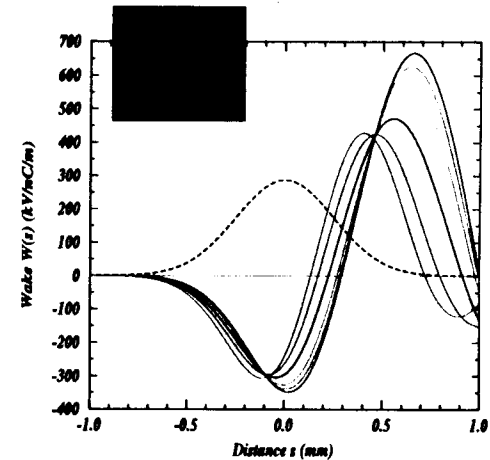
Bunch 250μ Tube: $R=5\text{mm}$, $\langle H \rangle = \langle G \rangle = \langle T \rangle = 50 \mu$



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Surface roughness wake potential

- Here we have the transformation of the inductive wake potential to resistive potential with the length of the tube. The bunch has to pass the long enough distance to form this wake field.



Surface roughness wakefunction is just a resonator wakefunction with amplitude

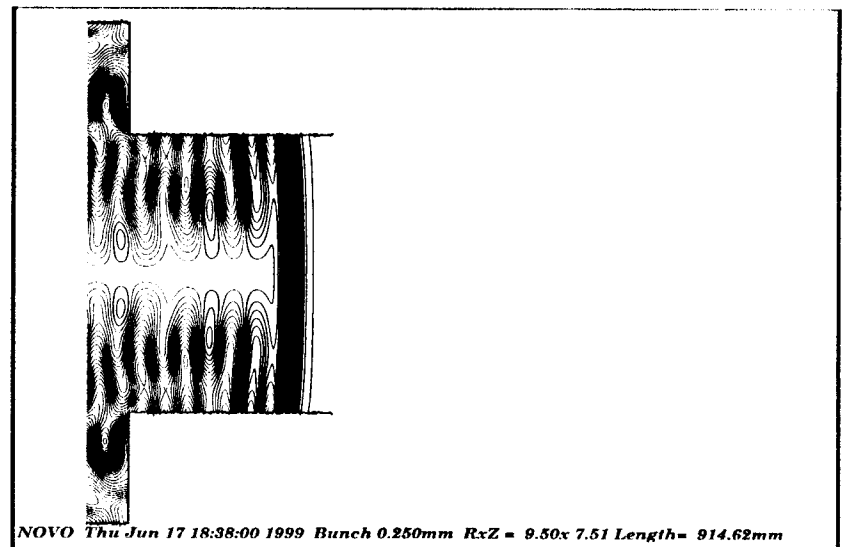
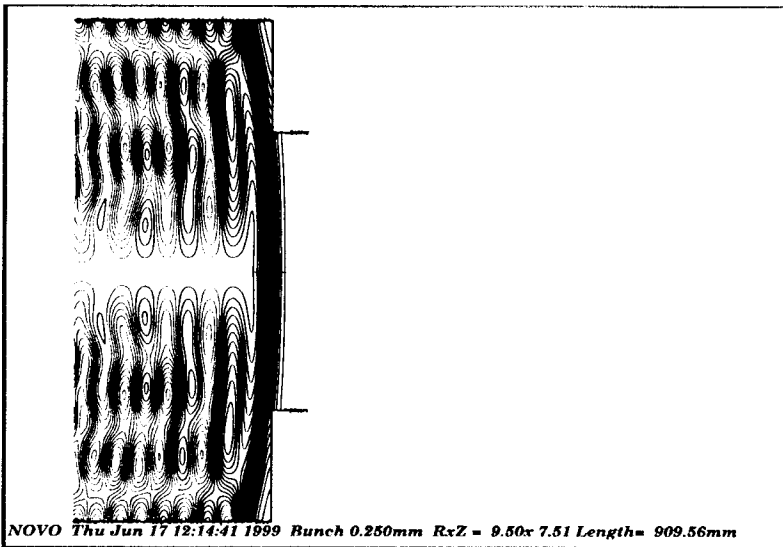
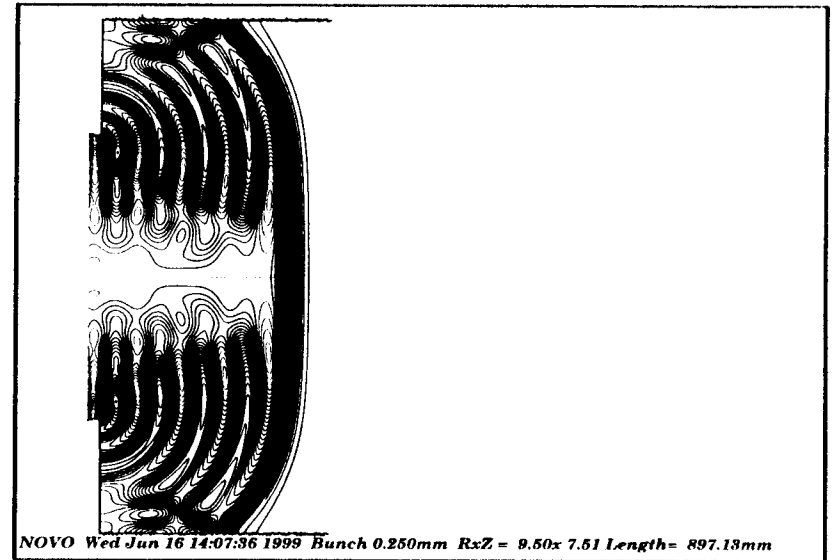
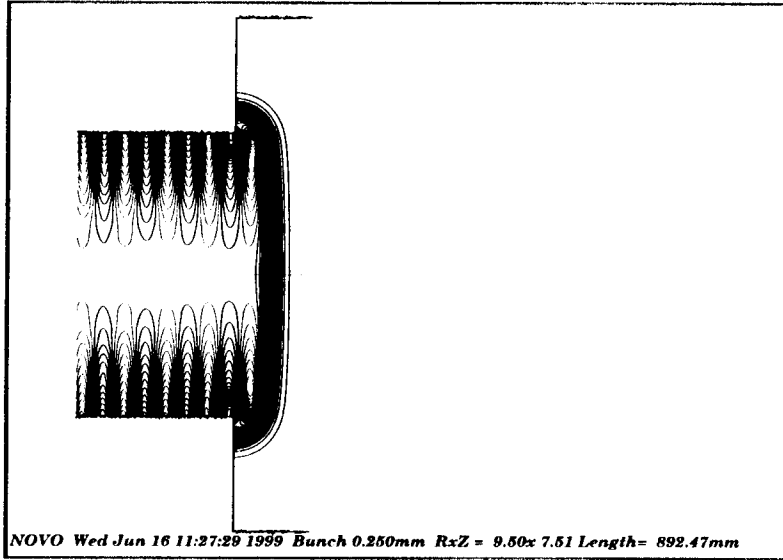
$$W_0 = \frac{Z_0 c}{\pi a^2} \quad \text{and frequency} \quad k \approx \frac{2}{\sqrt{a \delta}}$$

so the energy spread per unit length is

$$\Delta E_{wake} = q \frac{Z_0 c}{a \sigma_z^2} \frac{\delta}{4} \sqrt{\frac{1}{\pi 6 \sqrt{3}}}$$

Surface roughness wake field in the chamber transition

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Surface roughness and resistive wall wake fields

- The main part of the resistive wake function is also described by a resonator wake function of $Q=1$ with the same amplitude

$$W_0 = \frac{Z_0 c}{\pi a^2}$$

- but more higher frequency

$$k_Q = \sqrt{3} \left(\frac{\sigma_c}{2ca^2} \right)^{1/3}$$

- so the surface roughness fields are stronger if the effective roughness size

$$\delta > \frac{4}{3} \sqrt[3]{a} \left(\frac{c}{2\pi\sigma_c} \right)^{2/3}$$

Estimation for the energy spread from a pumping slot

- The effective „roughness“ size of a round slot with radius h can be estimated by
- Assuming that slots are situated at the distance of $2h$ from each other we can estimate the number of slots on the perimeter of the tube
- Then one slot will give the energy spread

$$\delta = \frac{h}{\pi}$$

$$M = \frac{2\pi a}{2h}$$

$$\Delta E_{slot} = g \frac{Z_0 c}{\sigma^2} \frac{1}{2\pi^2} \frac{h^3}{a^2} \sqrt{\frac{1}{\pi 6\sqrt{3}}}$$

- Comparison with known formula shows the coherent effect of slots

Fokker-Planck Equation

- Distribution function $f(t,x,p)$

$$\frac{\partial}{\partial t} f + \dot{x} \frac{\partial}{\partial x} f + \dot{p} \frac{\partial}{\partial p} f = \lambda \frac{\partial}{\partial p} \left\{ p f + \frac{\partial}{\partial p} f \right\}$$

$$\dot{x} = p$$

$$\dot{p} = -x + I_0 W(t, x)$$

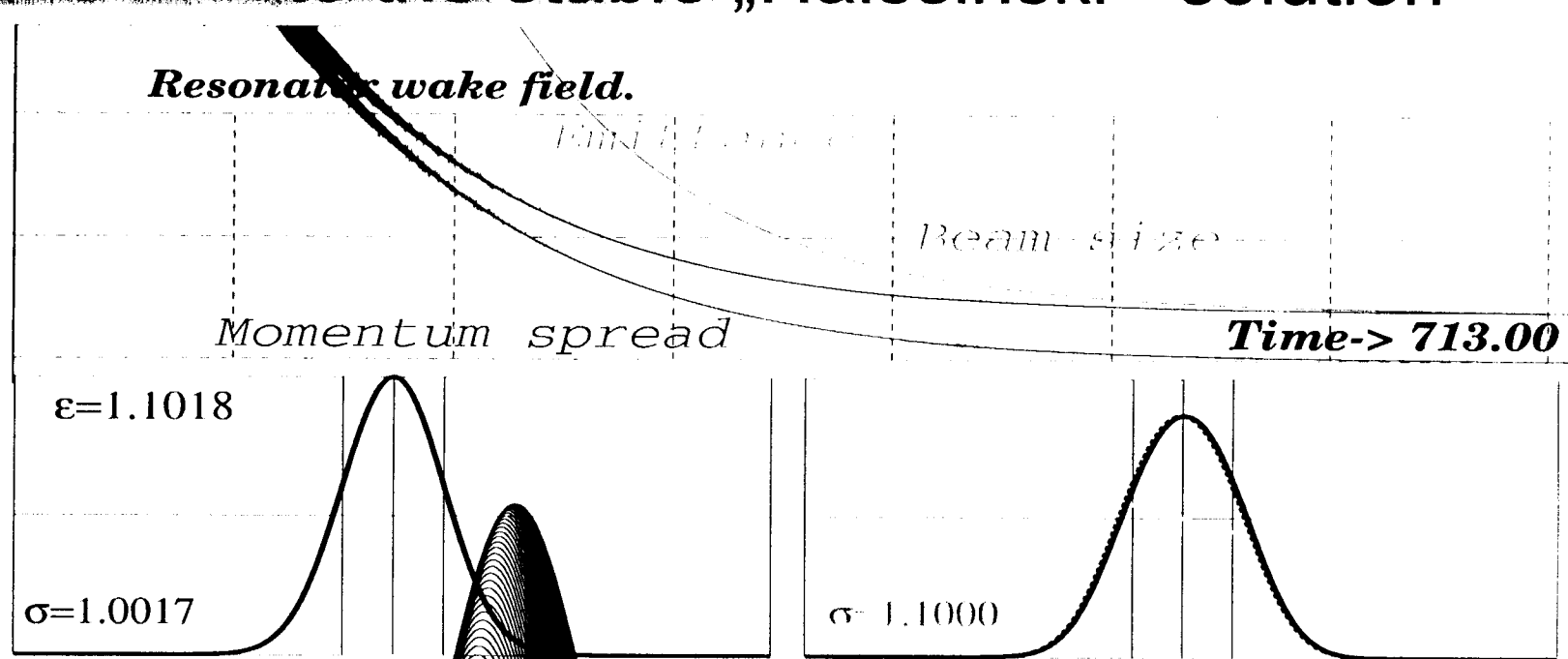
- Time is measured in synchrotron periods
- Coordinate and momentum are normalized by the length and momentum spread of a bunch of small intensity

Numerical simulation

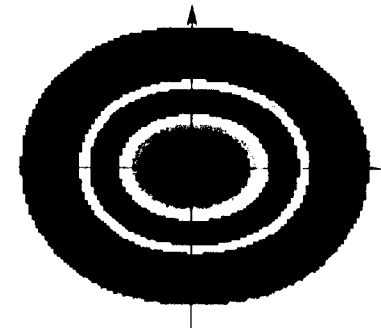
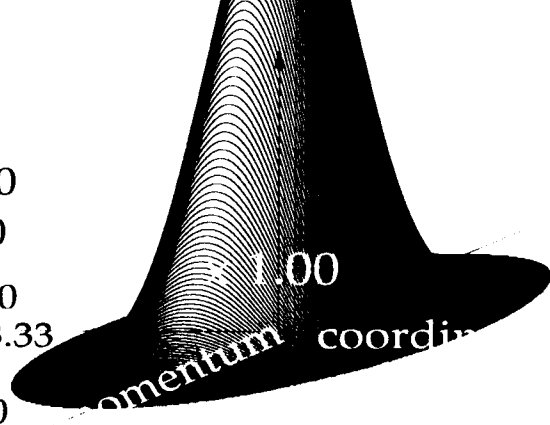
- Original implicit finite-difference algorithm
- Correct dispersion relation (up to the meshsize wavelength)
- No numerical diffusion, distortion or modulation
- TEST: Damped synchrotron oscillations to the stable solution of Haissinski equation. High-frequency wake field $\kappa\sigma=25$
- COMPARISON with the results of multi-particle tracking simulations (R.Baartman and M.D'yachkov, 1996). Low-frequency wake field $\kappa\sigma=0.5$

Damped synchrotron oscillations to the stable „Haissinski“ solution

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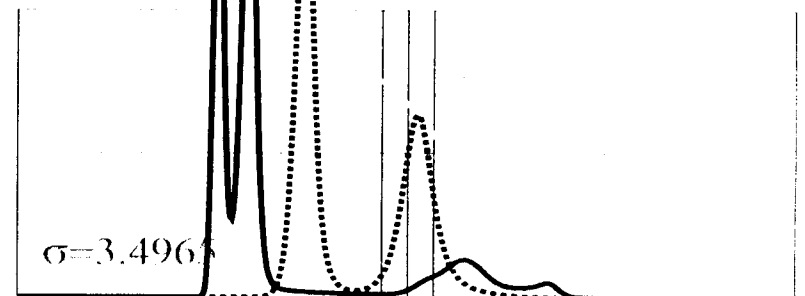
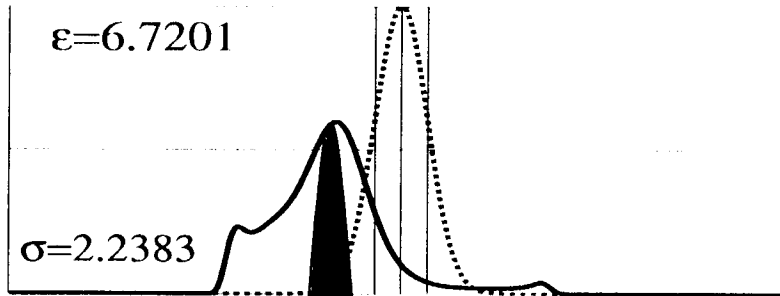
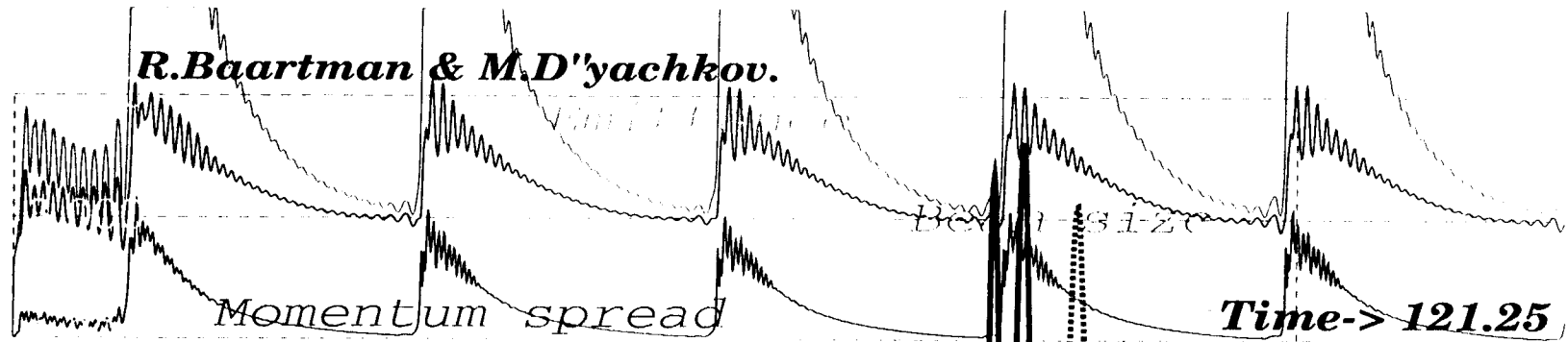


K= 25.000
I=1000.0
Q=1000.0
Damp=200.0
mod=0.0100
NxN=500x500
N/sigma= 33.33
TET=0.0010
Konto=1.0000



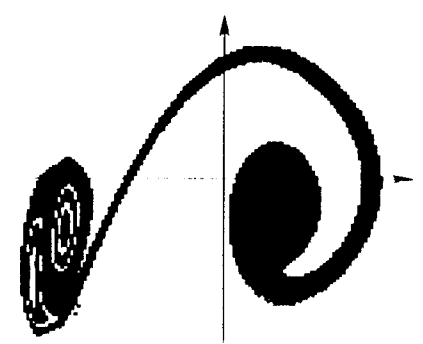
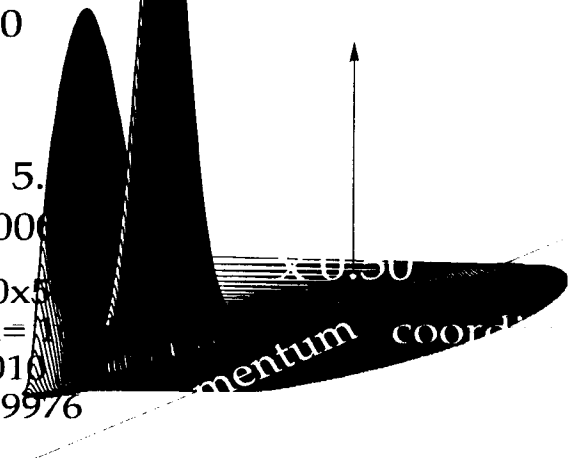
Comparison with Tracking Simulations

R. Baartman & M. D'yachkov.



K= 0.500
I= 30.0
Q= 1.0
Damp= 5.
mod=0.000

NxN=500x500
N/sigma=500
TET=0.0010
Konto=0.9976



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Longitudinal Instability

Dimensionless intensity parameter

$$I_0 = \frac{q W_0 c}{V_{rf} \omega_{rf} \sigma_0}$$

1. Bunch lengthening. Stable solution of Haissinski equation.

$$\sigma > 1 \quad \delta p = 1$$

2. Microwave instability. Small oscillations of bunch length.

$$\sigma > 1 \quad \delta p > 1$$

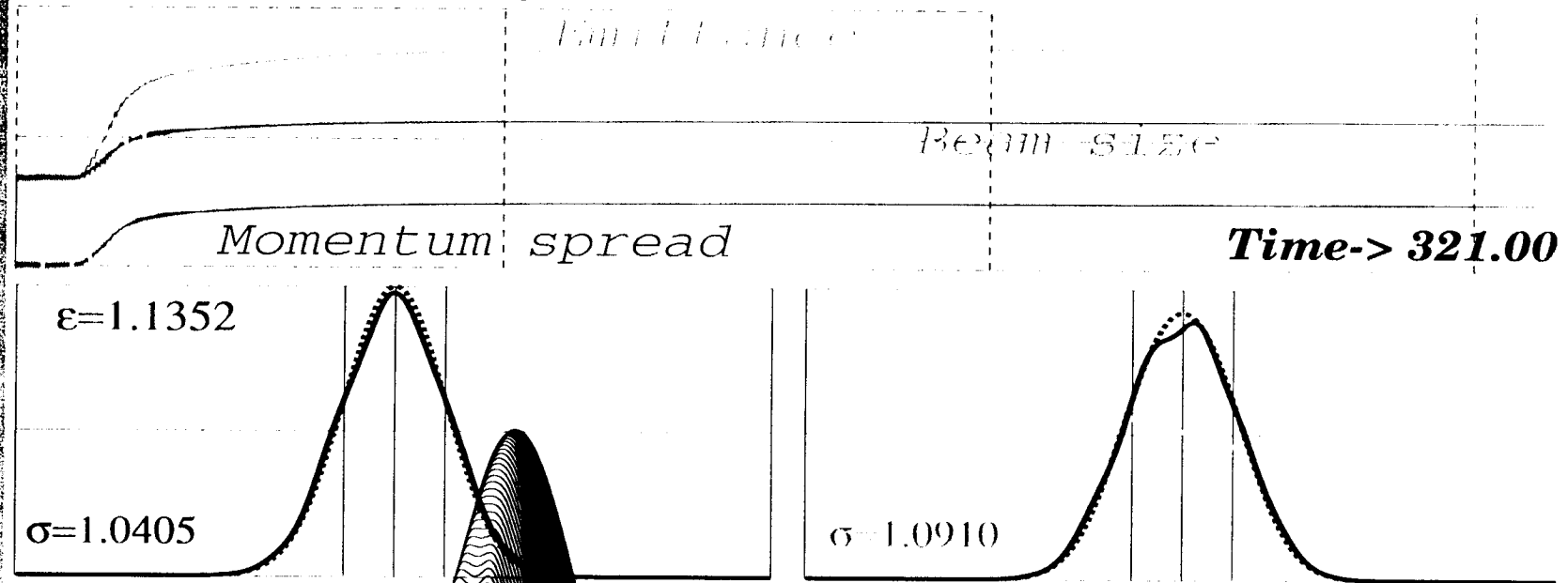
3. Large oscillations of bunch length.

4. Sawtooth oscillations.

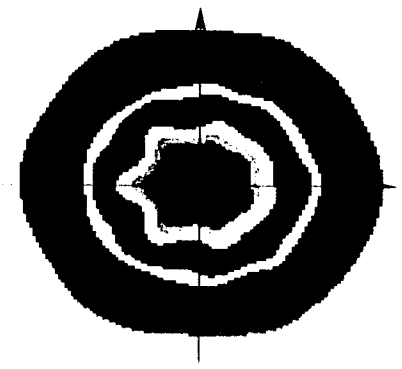
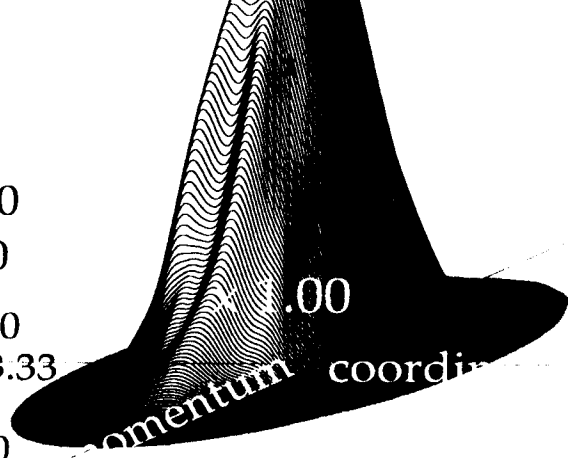
Microwave instability. Small oscillations.

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Resonator wake field.

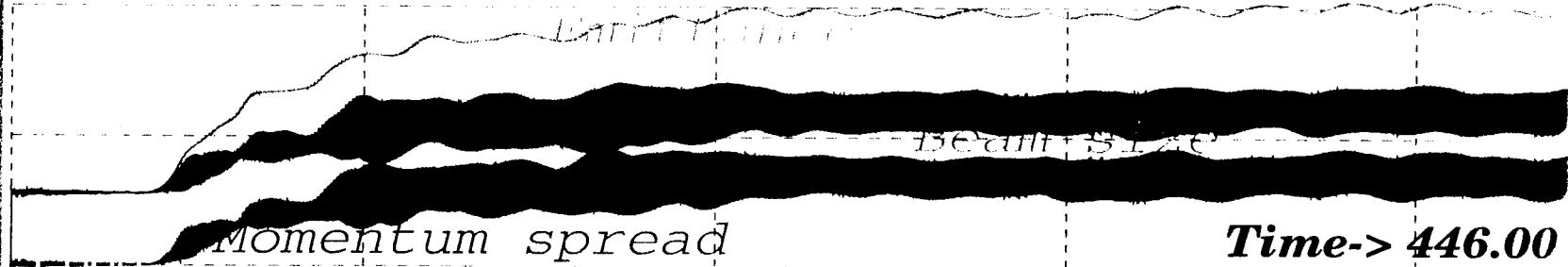


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Q=1000.0
Damp=100.0
mod=0.0000
NxN=500x500
N/sigma= 33.33
TET=0.0010
Konto=1.0000

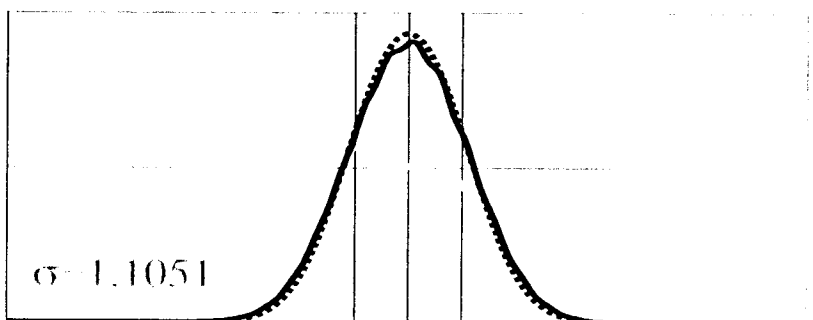
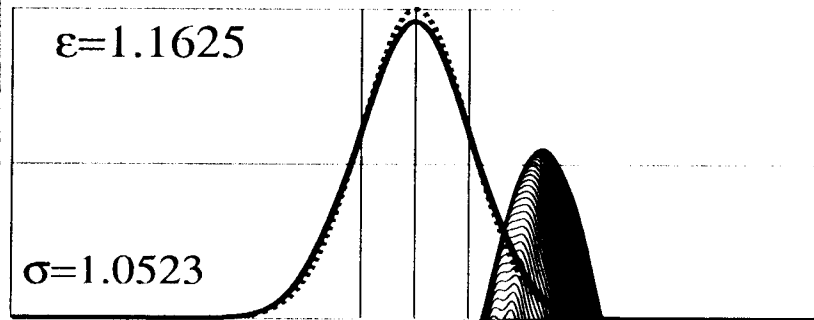


Microwave Instability. Large oscillations.

Resonator wake field.

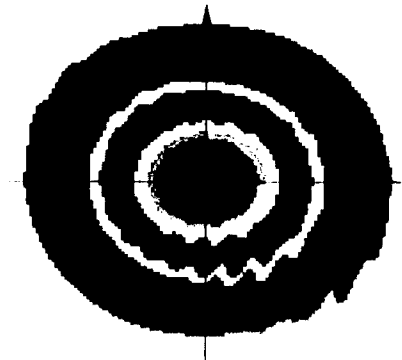
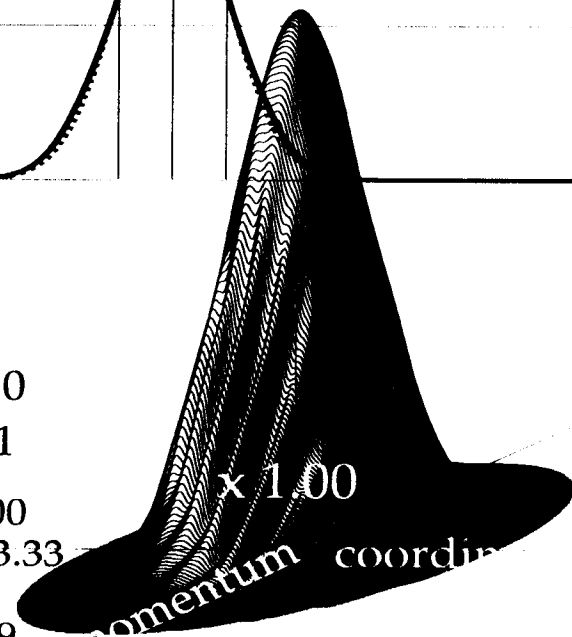


Momentum spread



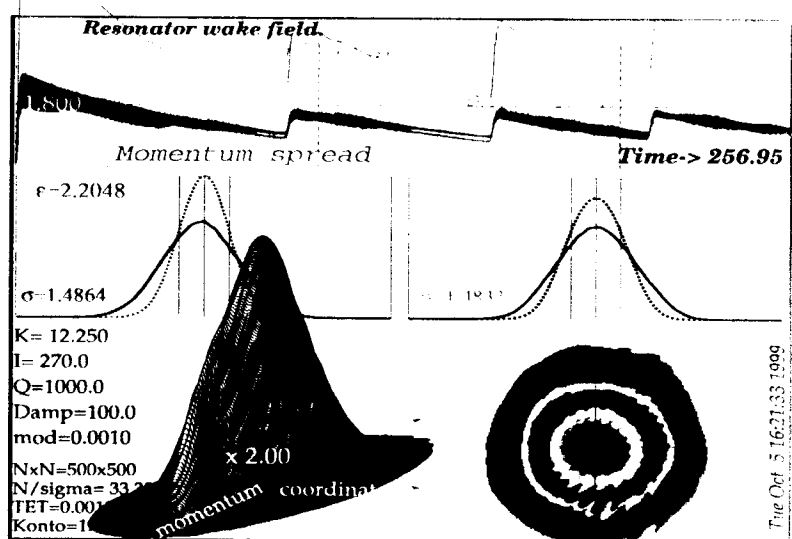
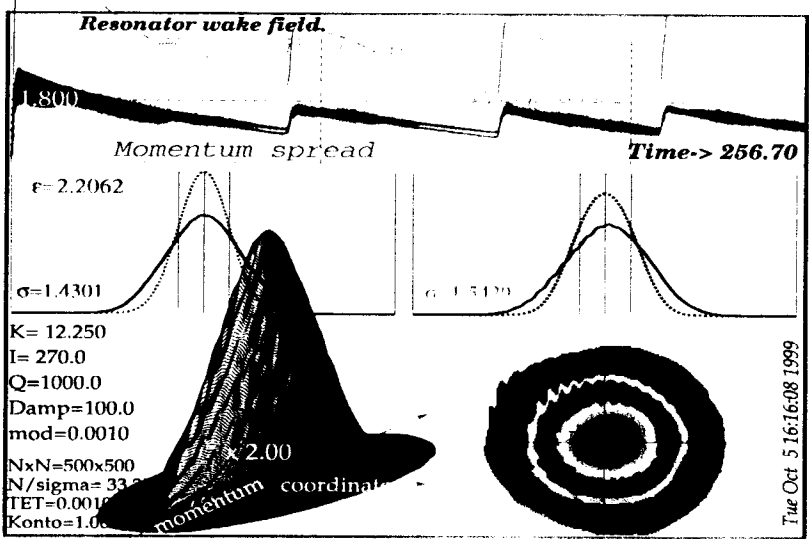
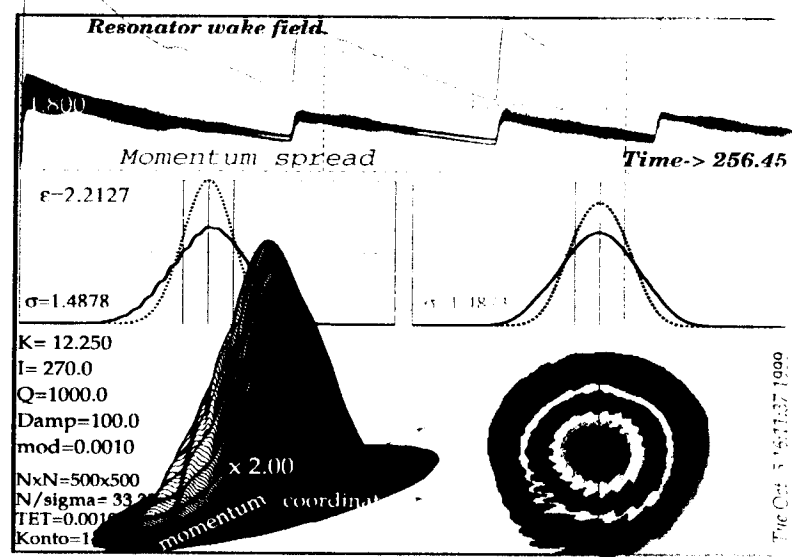
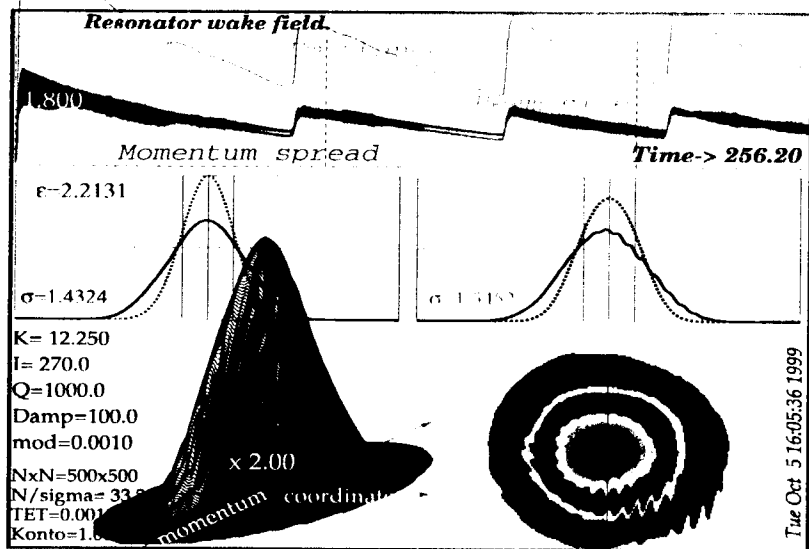
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TET=0.0010
Konto=1.0089



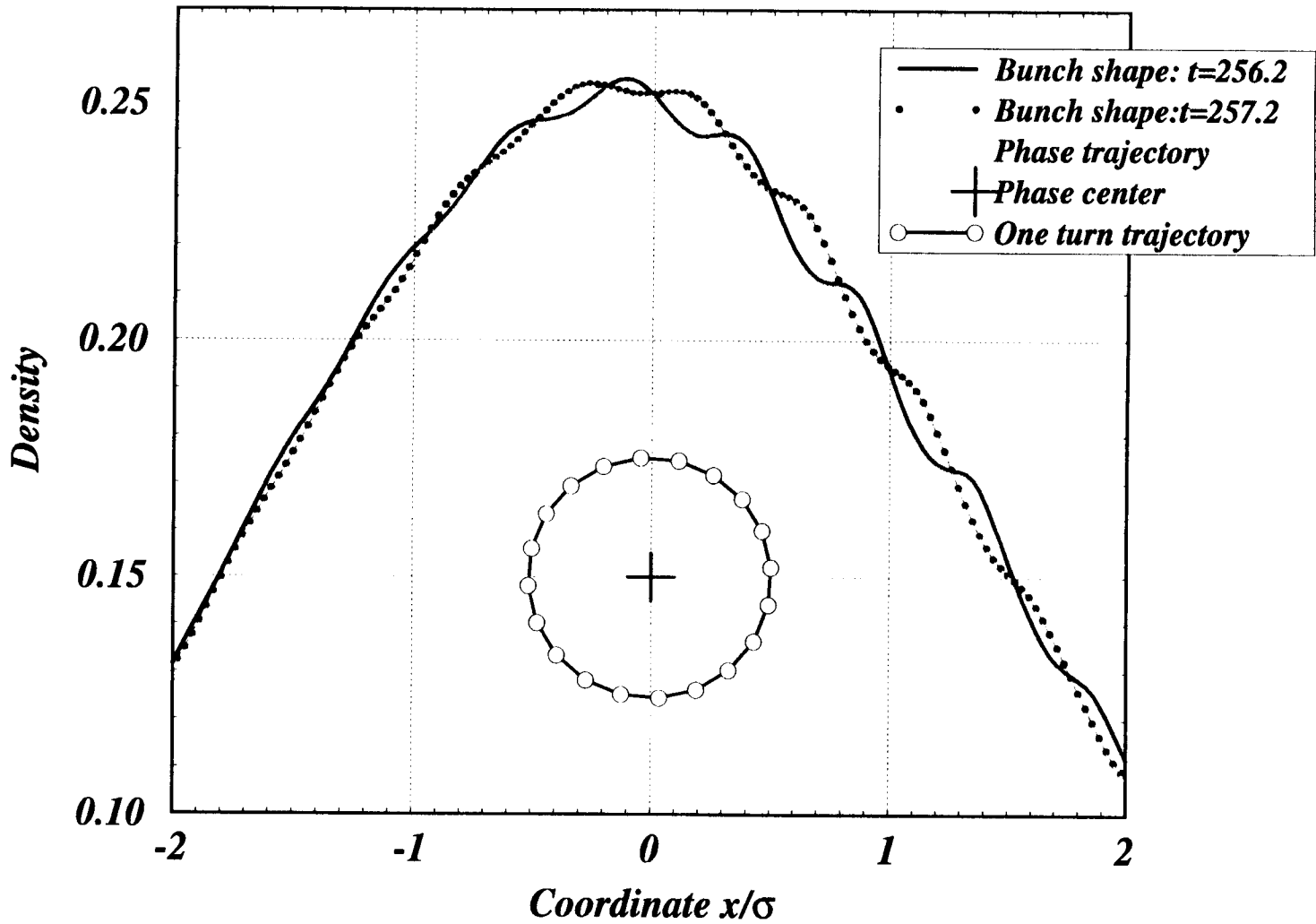
Sawtooth instability behaviour during the damping period.

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Bunch shape and bunch center phase trajectory during the damping period.

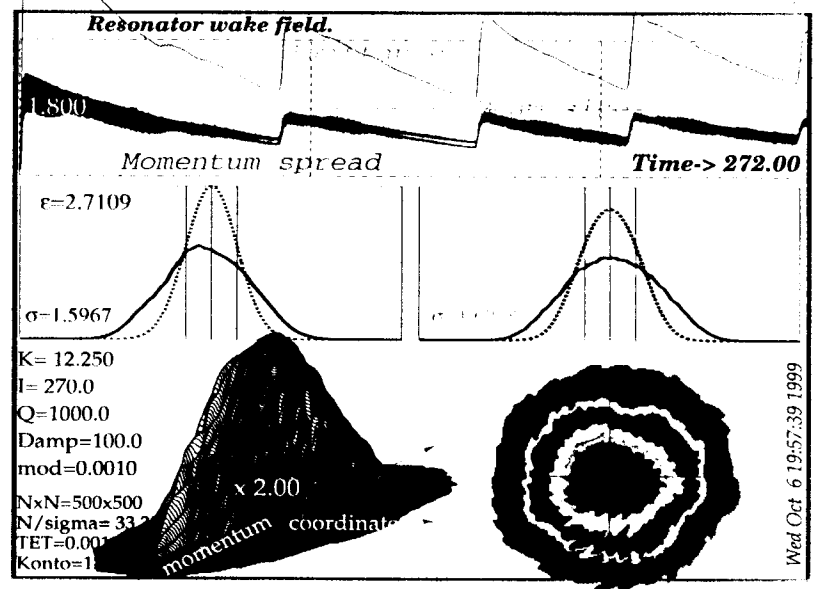
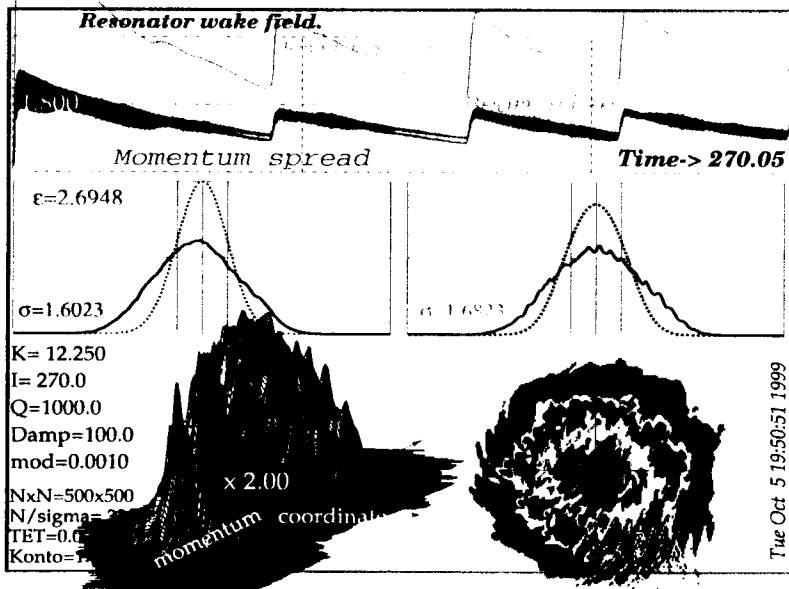
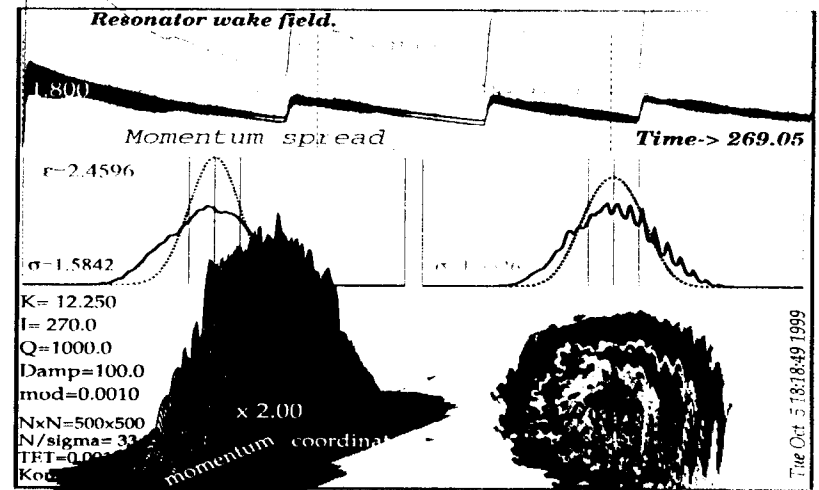
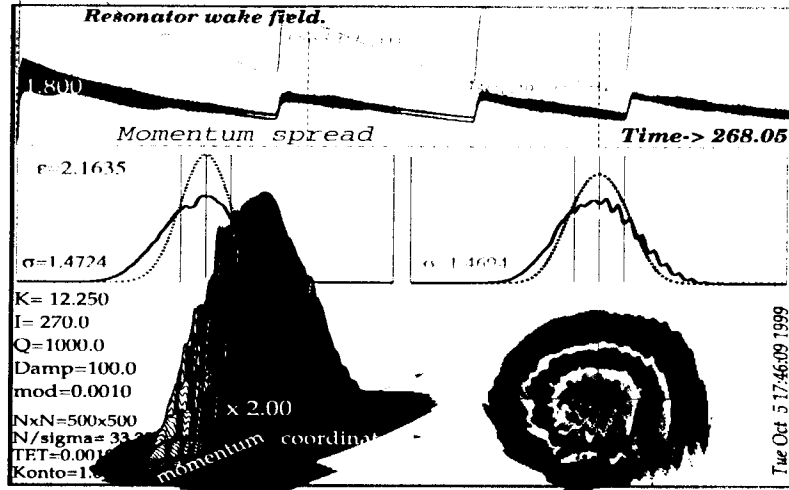
Bunch shape demodulation



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Sawtooth instability behaviour during the blow-up period

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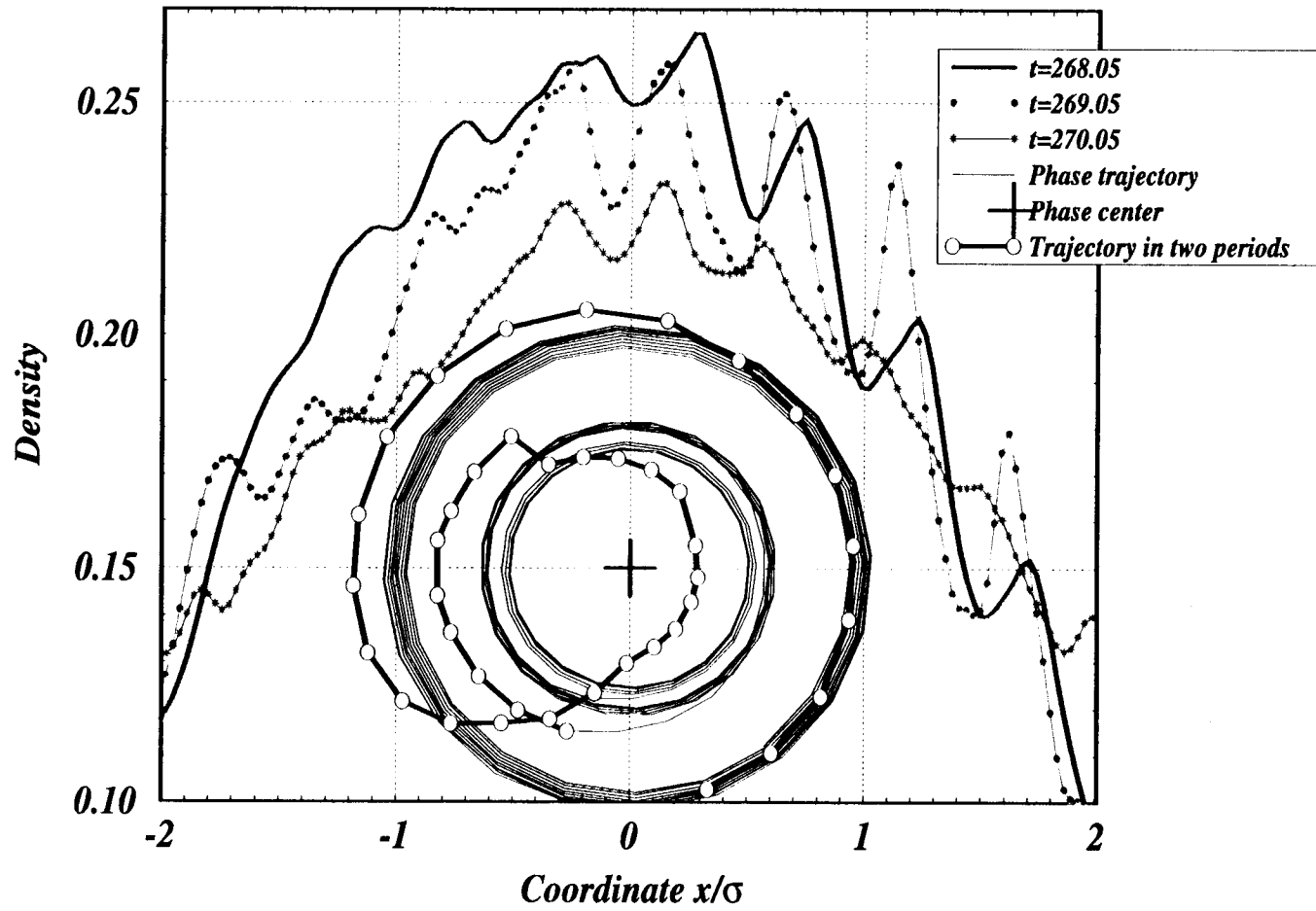


Blow-up period

● Bunch shape and phase trajectory

Bunch shape in two synchrotron periods

Bunch center phase trajectory in blow-up period



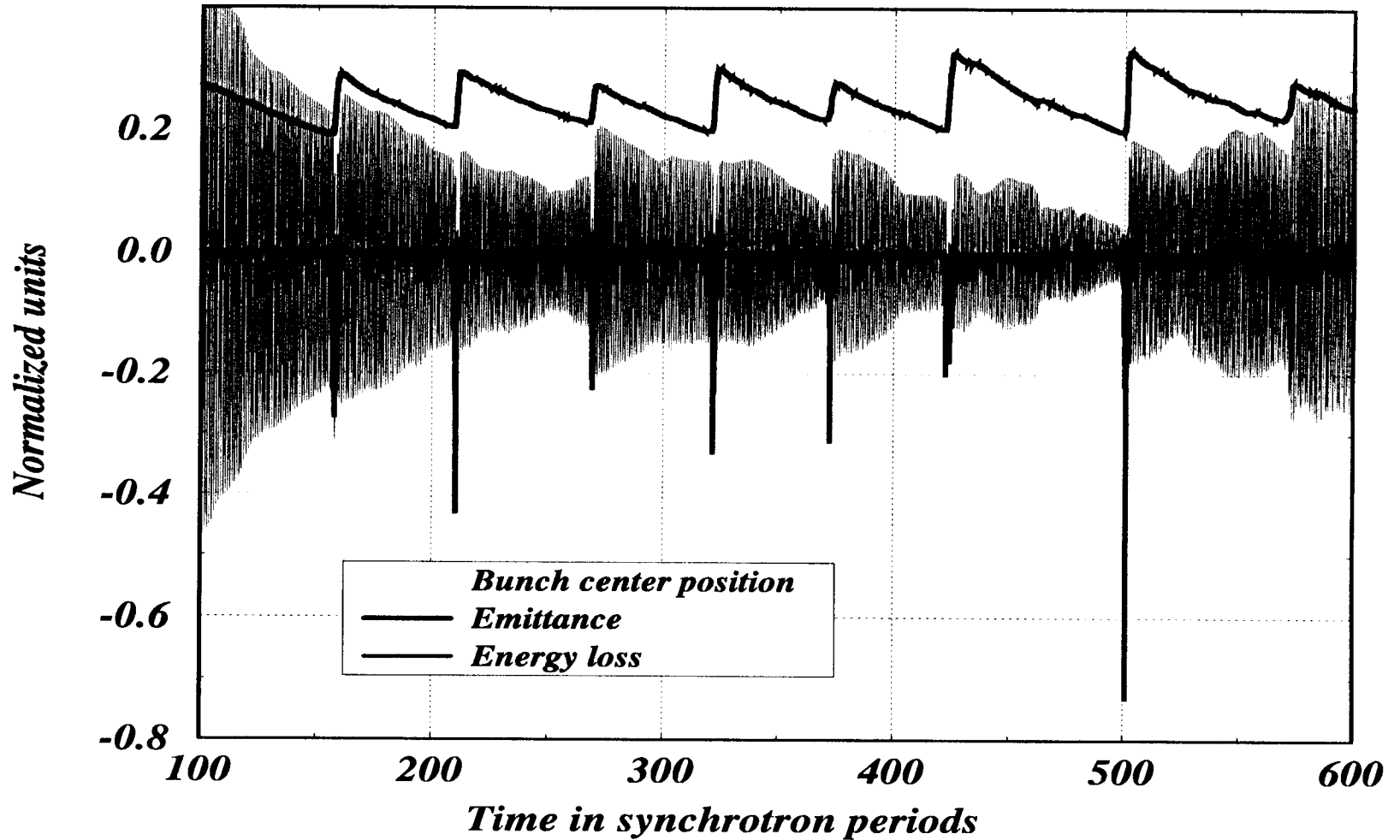
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Stochastic bursts of radiation

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Bunch center position, Emittance and Energy loss

K=12.25 I=270, Damp.time=100



Saw Tooth Instability Behaviour

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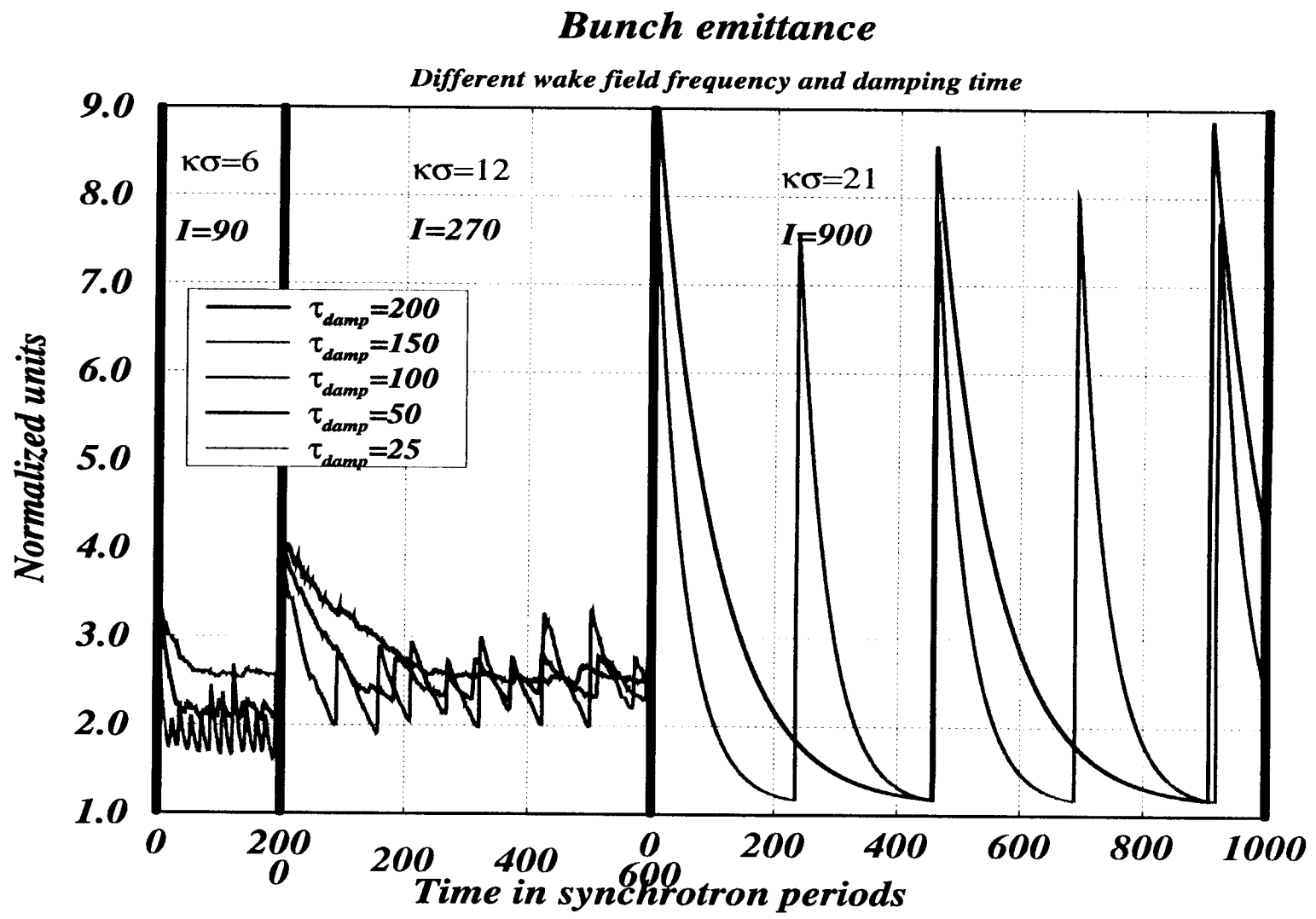
- Damping period
 - ◆ Adiabatic transition
 - ◆ Anti-resonance microbunching, 180° phase shift with each synchrotron period

- Blow-up period
 - ◆ „Metastable“ states
 - ◆ „Quick“ transition (resonance microbunching)
 - ◆ Stochastic bursts of radiation in the transition

- „Quantum“ behaviour?

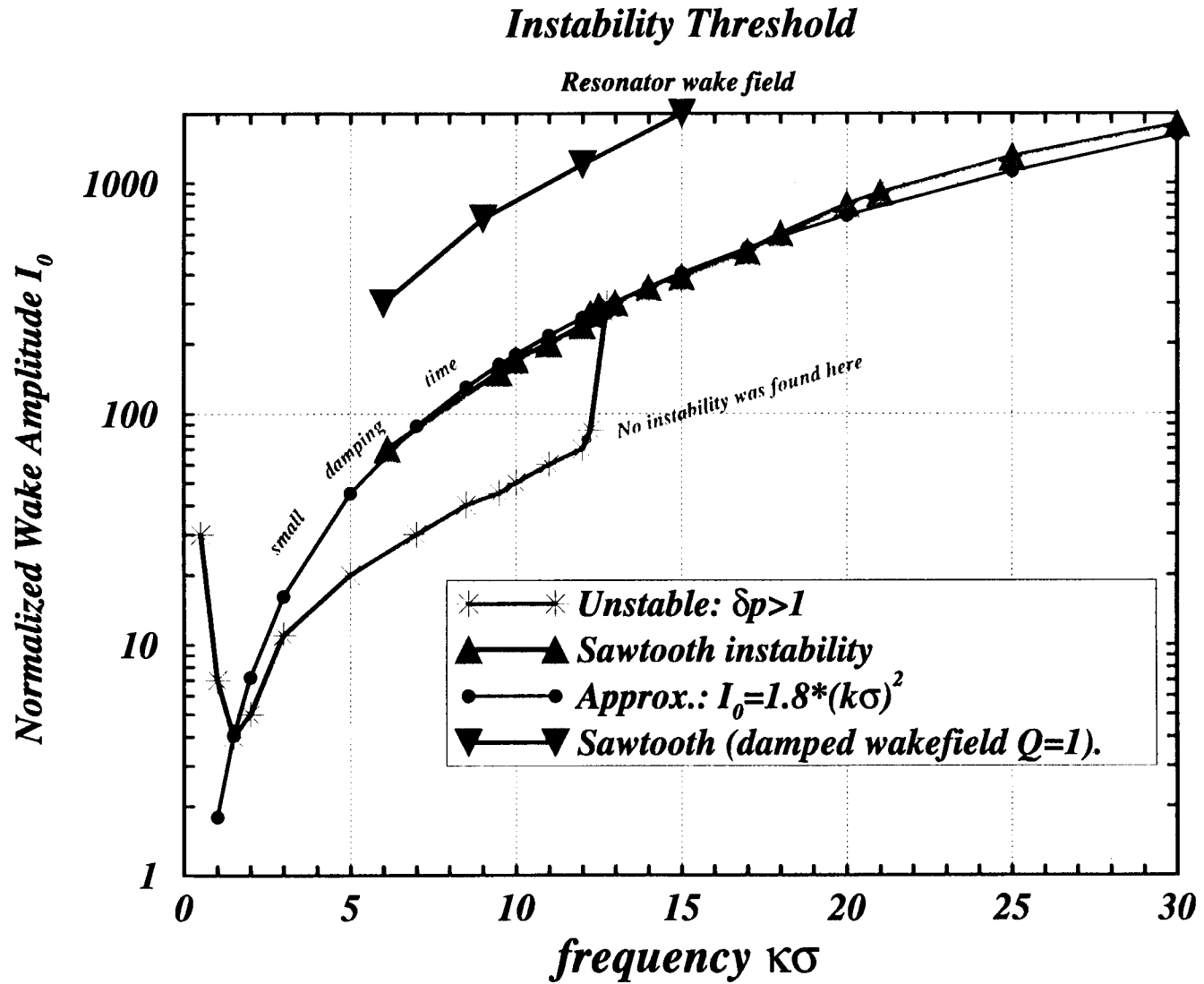
Sawtooth instability and damping time

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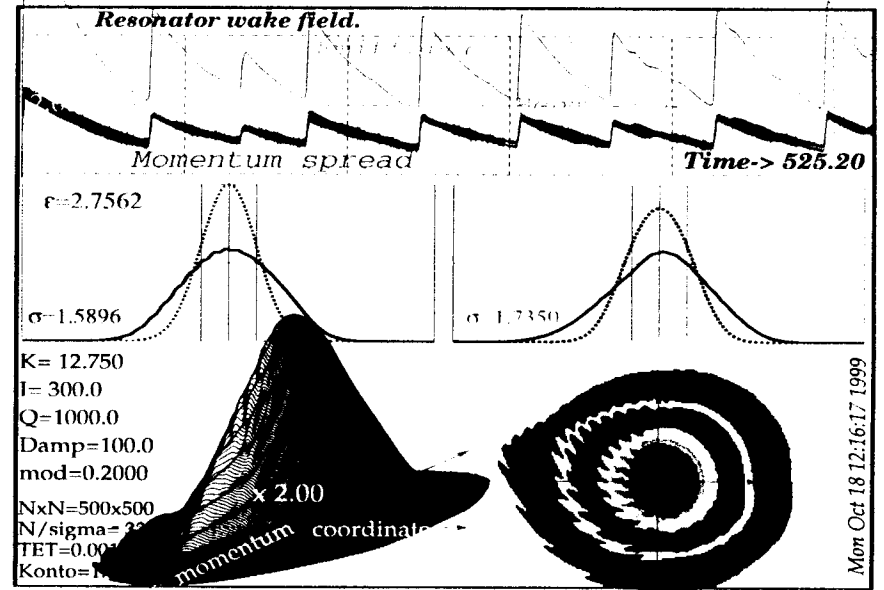
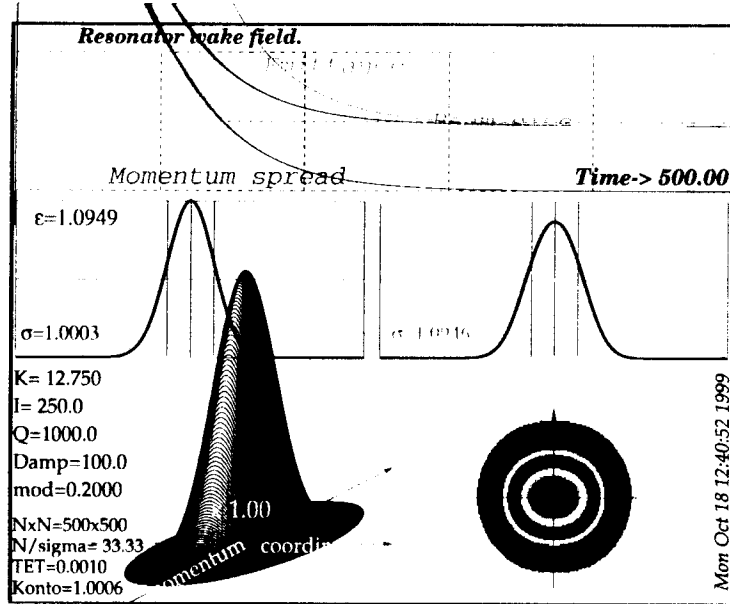
Instability threshold

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No intermediate state. Instability comes by 25% of additional charge

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- Threshold for a bunch charge (for sawtooth instability)

- ◆ Estimation
$$I_{thr} \approx \left(\frac{6\sqrt{3}}{\pi} \right)^{1/2} (k\sigma_z)^2 = 1.8(k\sigma_z)^2$$

- ◆ means that
- ◆ instability starts when the wake energy spread becomes comparable with the RF focusing

$$\Delta E_{wake} \approx \left[V_{RF} \frac{\omega_{RF}}{c} \sigma_z \right]$$

Estimation and Example

- ◆ Introducing a „roughness“ parameter for the vacuum chamber „wake“ description 

- ◆ we can give an estimation for the threshold of the bunch charge

$$q_{thr} \approx 3.6 \eta h_{RF} \frac{V_{RF}}{Z_0} \frac{\sigma_z}{c} \left(\frac{\sigma_z}{R} \right)^2$$

- ◆ Example. Assuming that damping ring has the following parameters:

- RF voltage $V_{RF} = 800kV$ Harmonic number $h_{RF} = 84$
- Bunch length $\sigma_z = 5mm$ Effective radius of a ring $R = 5.6m$

- ◆ and „roughness“ parameter $\eta = \frac{10}{1} \frac{1}{1\%} = 10^3$

- ◆ we can get estimation for the charge $q_{thr} = 8.4nC$



Summary

- Simulation study of the longitudinal bunch instability was performed for the very high frequency wake fields, that are usually described by the inductive impedance.
- The Fokker-Planck equation for the phase space distribution is solved numerically by using the original implicit finite-difference method.
- It was found that in the high frequency range the bunch instability has mainly „sawtooth“ character and is accompanied by the bursts of coherent radiation, stochastically distributed in time..
- This effect has to be taken into consideration in the designs of the damping rings for the strong cooling of very high intensity bunches.