

1

EVALUATION OF GROUND MOTION

& VIBRATION ON LINEAR COLLIDERS

GROUND MOTION IN FUTURE ACCELERATORS

ICFA WORKSHOP

NOV. 8, 2000

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THIS WORK WAS (LARGELY) COMPLETED
IN 1995 —

COMBINED EFFORTS OF

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IS WRITTEN UP IN ZDR - SIAC REP. 474

VOL. 2. APPENDIX C P 1043

CHAP 11 GROUND MOTION P 71B -
(IN FINAL FORM)

$$P(\omega) \quad \mu m^2 / Hz \quad \langle \Delta y^2 \rangle = \int P(\omega) \frac{d\omega}{2\pi}$$

$$P(\omega) > 0$$

ny
ac

$$P(\omega, k_z)$$

$$P(\omega) = \int P(\omega, k) \frac{dk}{2\pi}$$

$$P(\omega, k) > 0$$



$$\mu(\omega, k) \equiv \frac{P(\omega, k)}{P(\omega)}$$

$$\int \mu(\omega, k) \frac{dk}{2\pi} = 1$$

$$\mu(\omega, k) > 0$$

→ μ a probability measure

→ $P(\omega)$ varies dramatically -

$\mu(\omega, k)$ "appears" to be constant -

VARIATION OF
POWER SPECTRUM
at Hiidenvesi

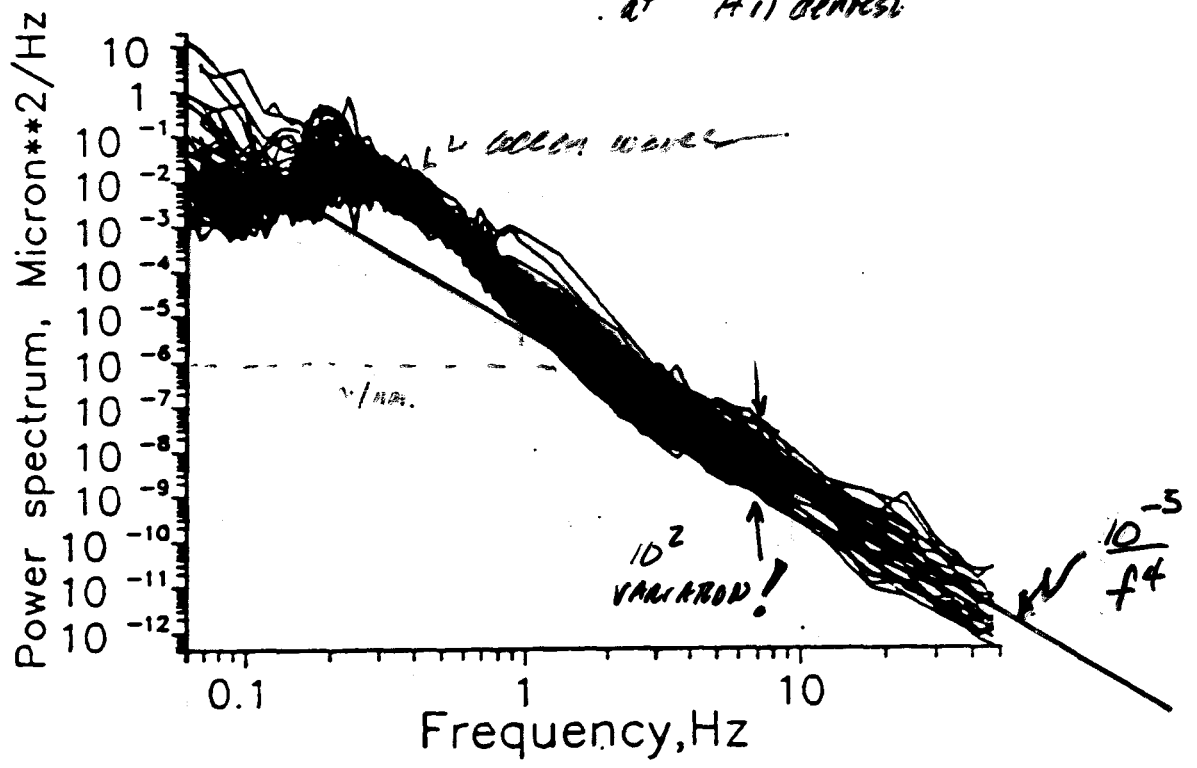
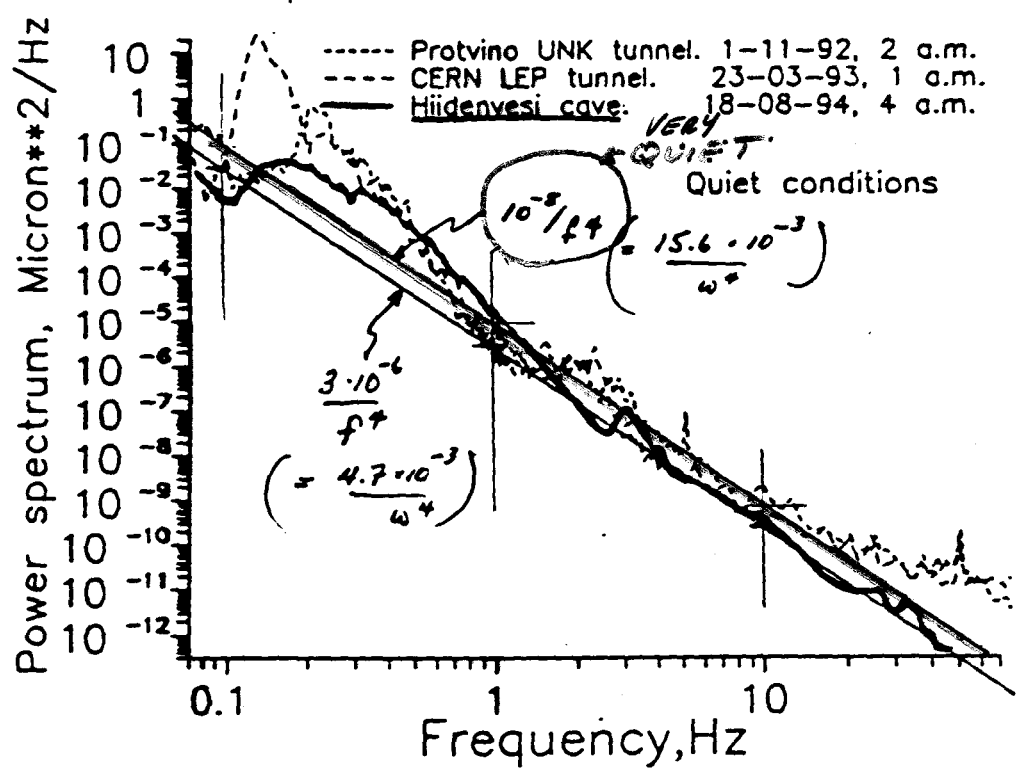
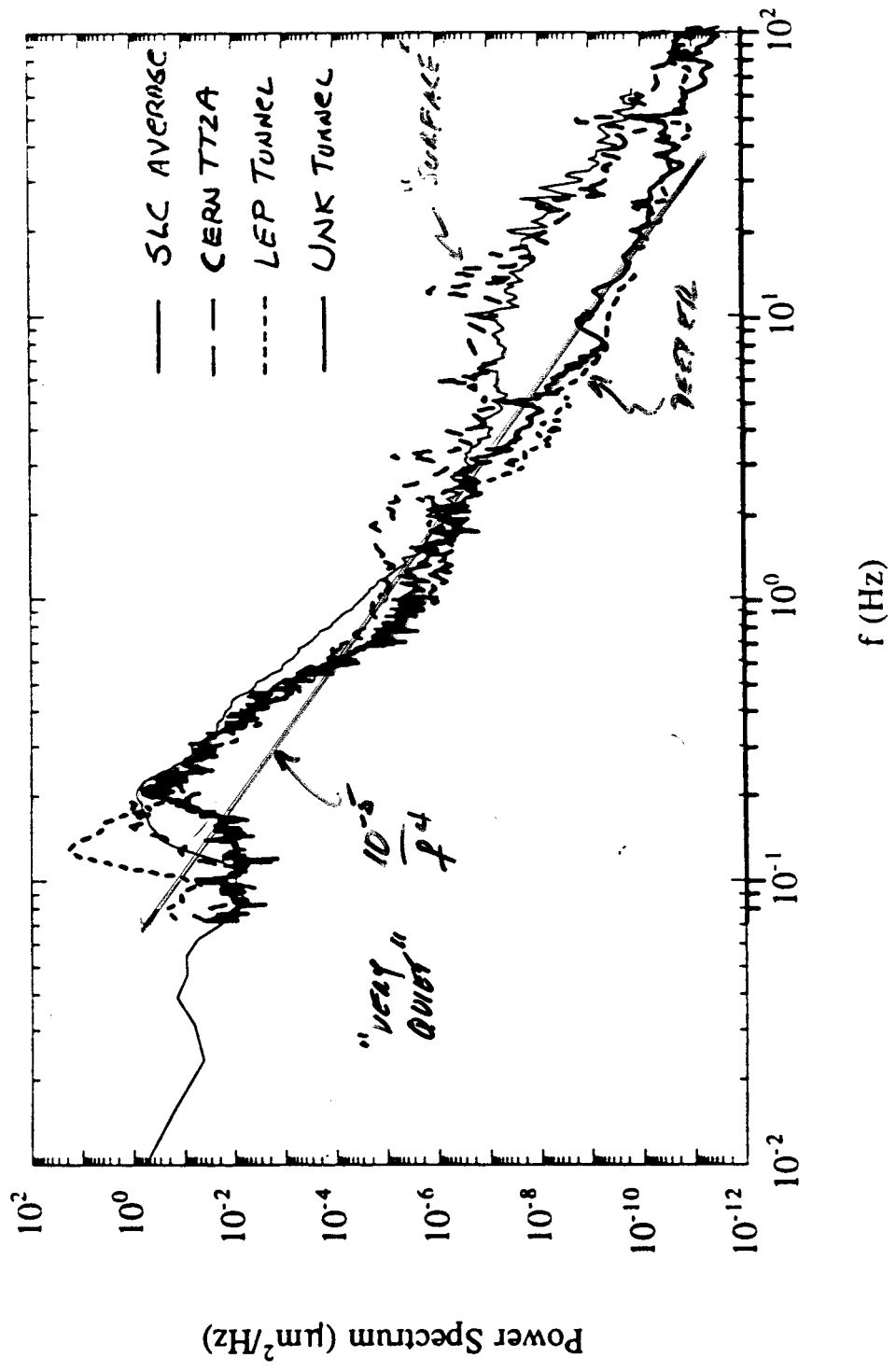


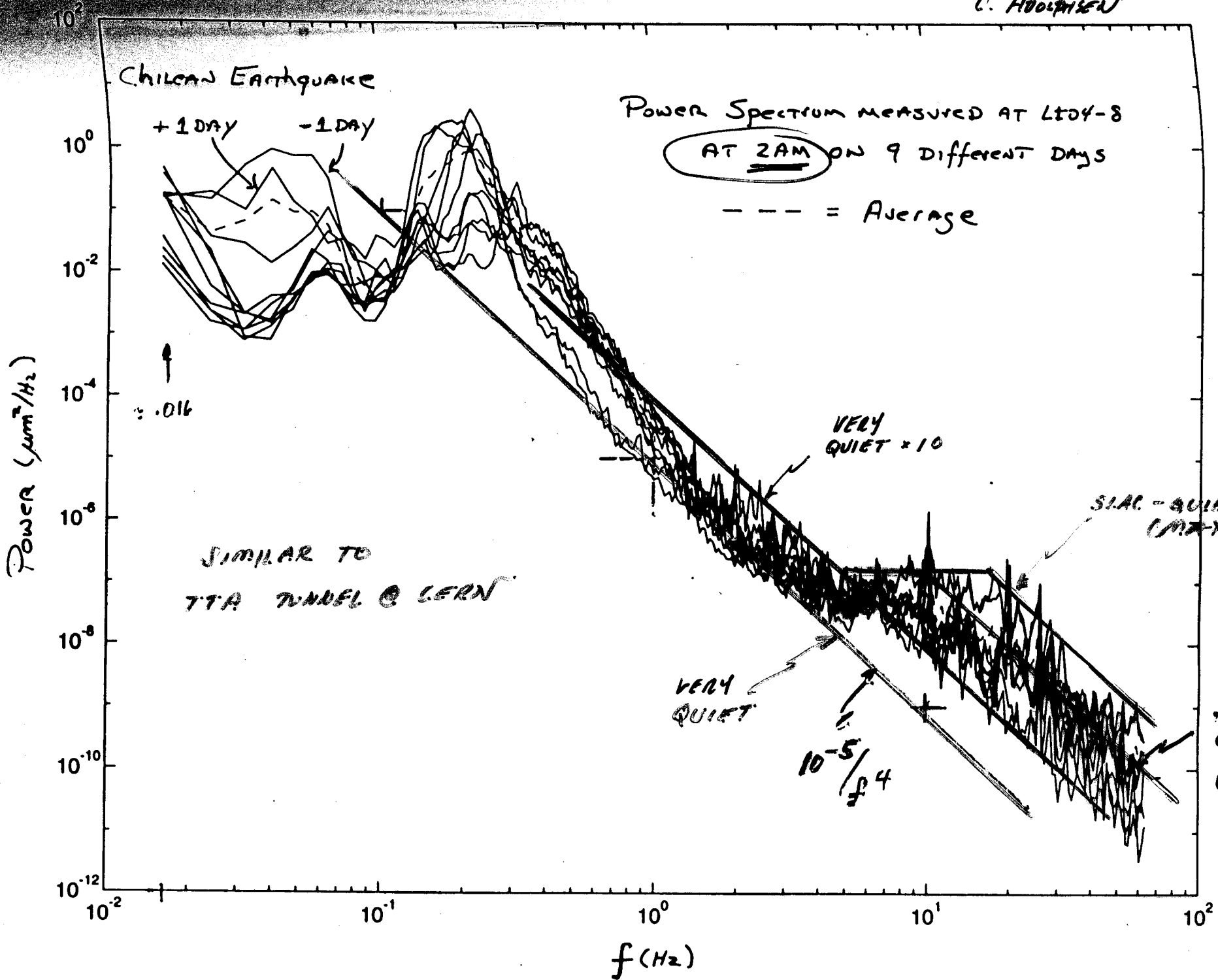
Fig.7. Variation of the power spectrum measured in Hiidenvesi in August 12-19, 1994.



A. SERV,
V. SMILTSEV, ..

Fig.2. Power spectra of vertical seismic vibrations measured in Russia (Protvino, UNK tunnel), in Switzerland (CERN LEP tunnel) [4] and in Finland (Hiidenvesi cave) in quiet conditions.





2.A.4

THE RATIO $R(\omega, \ell)$

7 (21)

$$\langle [y(t, s+\ell) - y(t, s)]^2 \rangle_s$$

$$= 2 \left[\int P(\omega) \frac{d\omega}{2\pi} - \iint P(\omega, k) \cos \omega k \ell \frac{dk}{2\pi} \frac{d\omega}{2\pi} \right]$$

$$= 2 \iint_0^\infty P(\omega, k) [1 - \cos \omega k \ell] \frac{dk}{2\pi} \frac{d\omega}{2\pi}$$

$$= 2 \int_0^\infty P(\omega) \frac{d\omega}{2\pi}$$

$$\boxed{\int_0^\infty \mu(\omega, k) [1 - \cos \omega k \ell] \frac{dk}{2\pi} = R(\omega, \ell)}$$

$$= 2 \int_0^\infty P(\omega) R(\omega, \ell) \frac{d\omega}{2\pi}$$

So SPECTRAL DENSITY OF $[y(t, s+\ell) - y(t, s)]^2$

is spectral density of $y(t, s)$

multiplied by

$$\frac{2 R(\omega, \ell)}{2\pi}$$

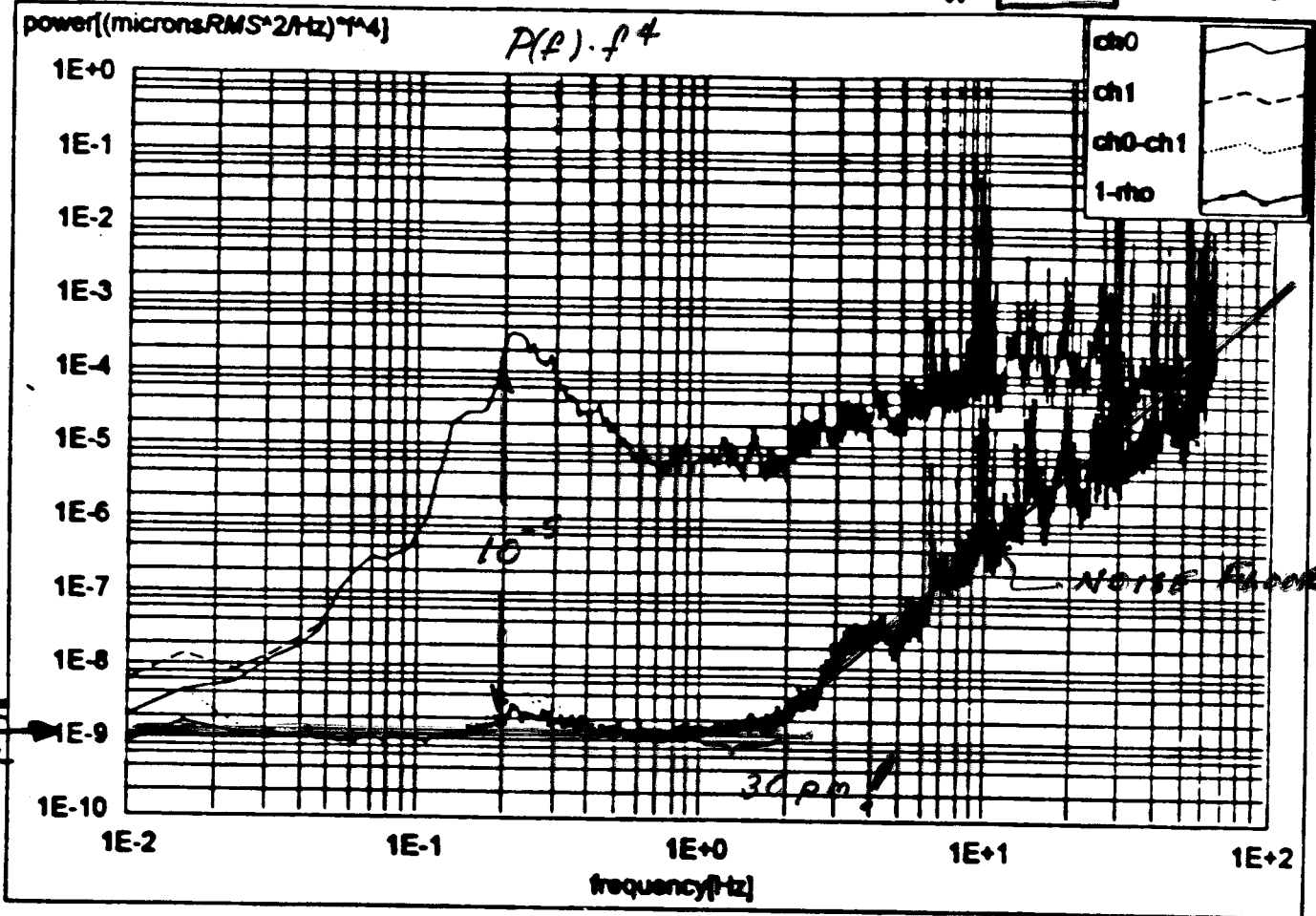
MEASURE $R \rightarrow$ EXTRACT μ

CAN GET THIS
DIRECTLY FROM
DATA.

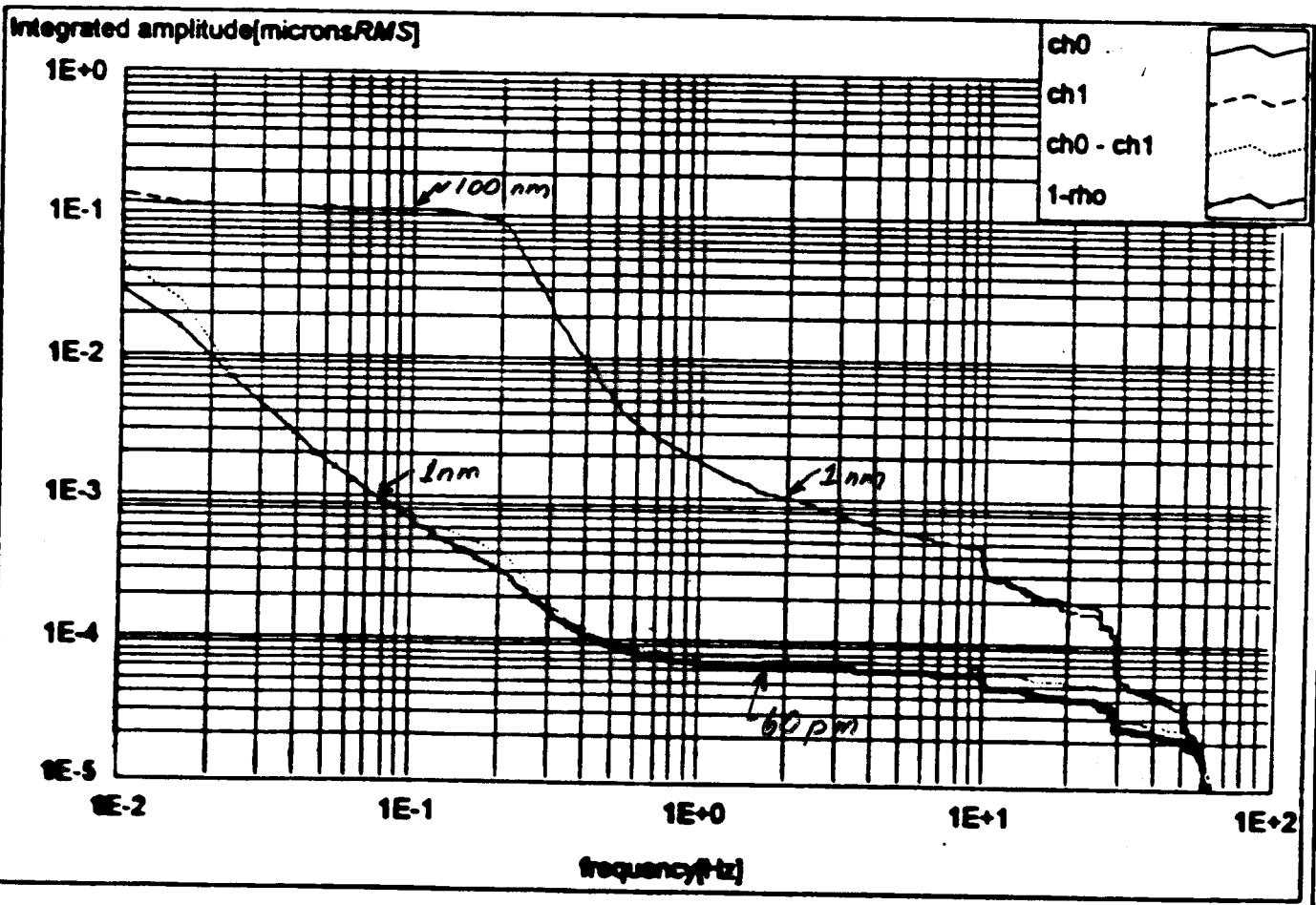
STS 2 MEASUREMENTS IN LTOF-8 WHEEL OFF $\Delta z = 0$

B

12C



loss
-20dB




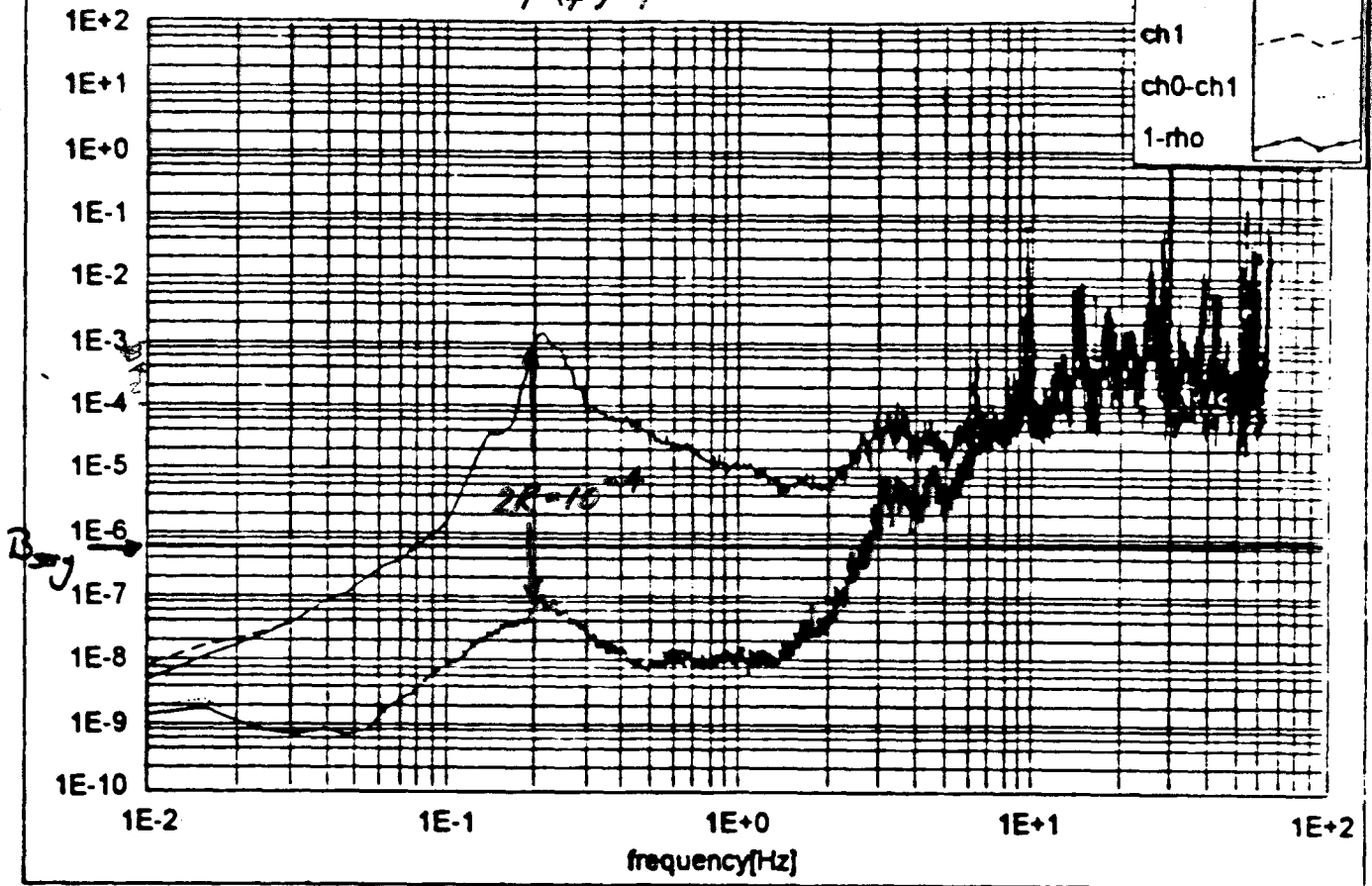
7 $\Delta z = 12 \mu$

5c

power[(micronsRMS²Hz)^{1/4}]


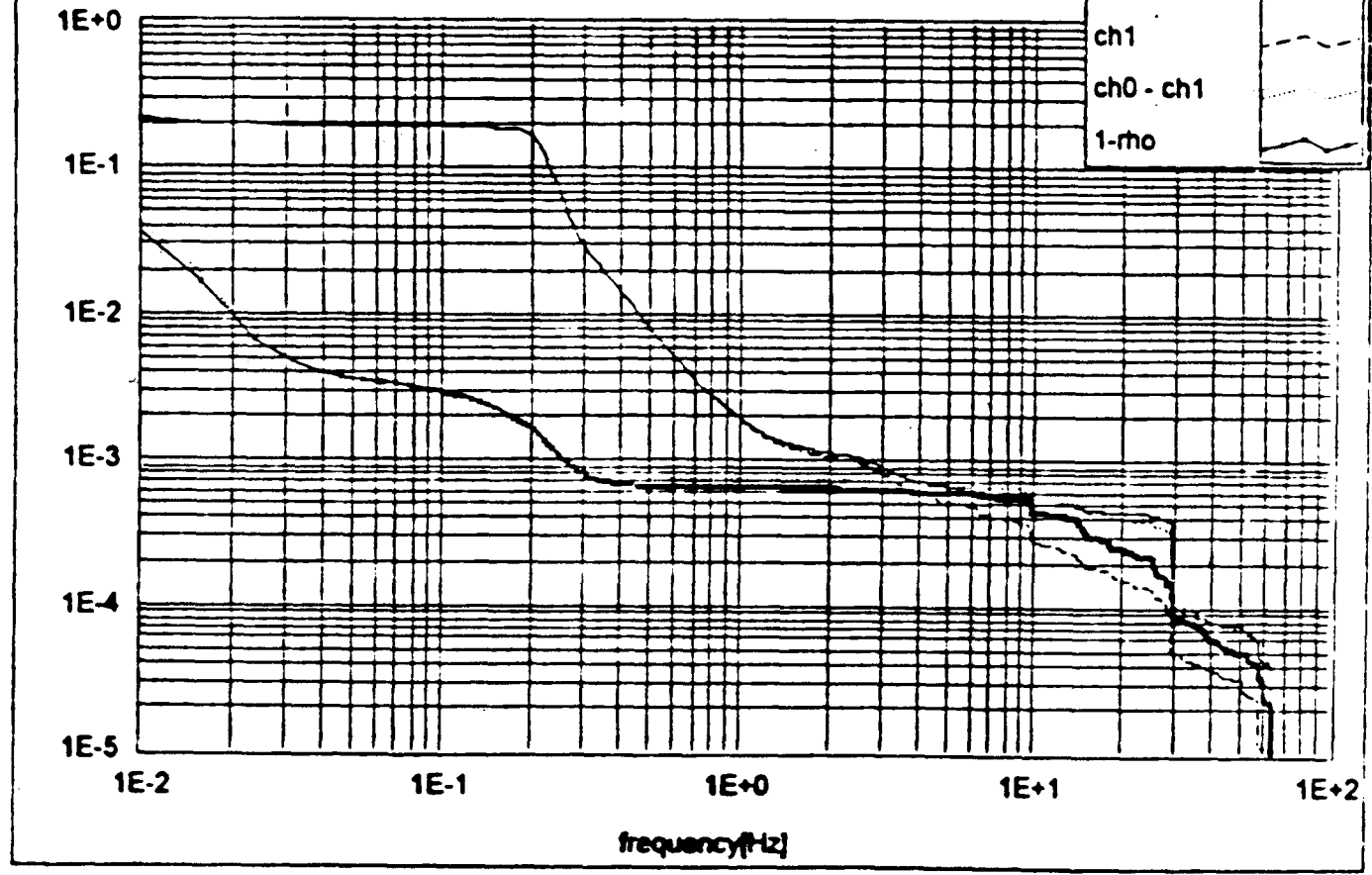
$P(f) \cdot f^4$

ch0
 ch1
 ch0-ch1
 1-rho

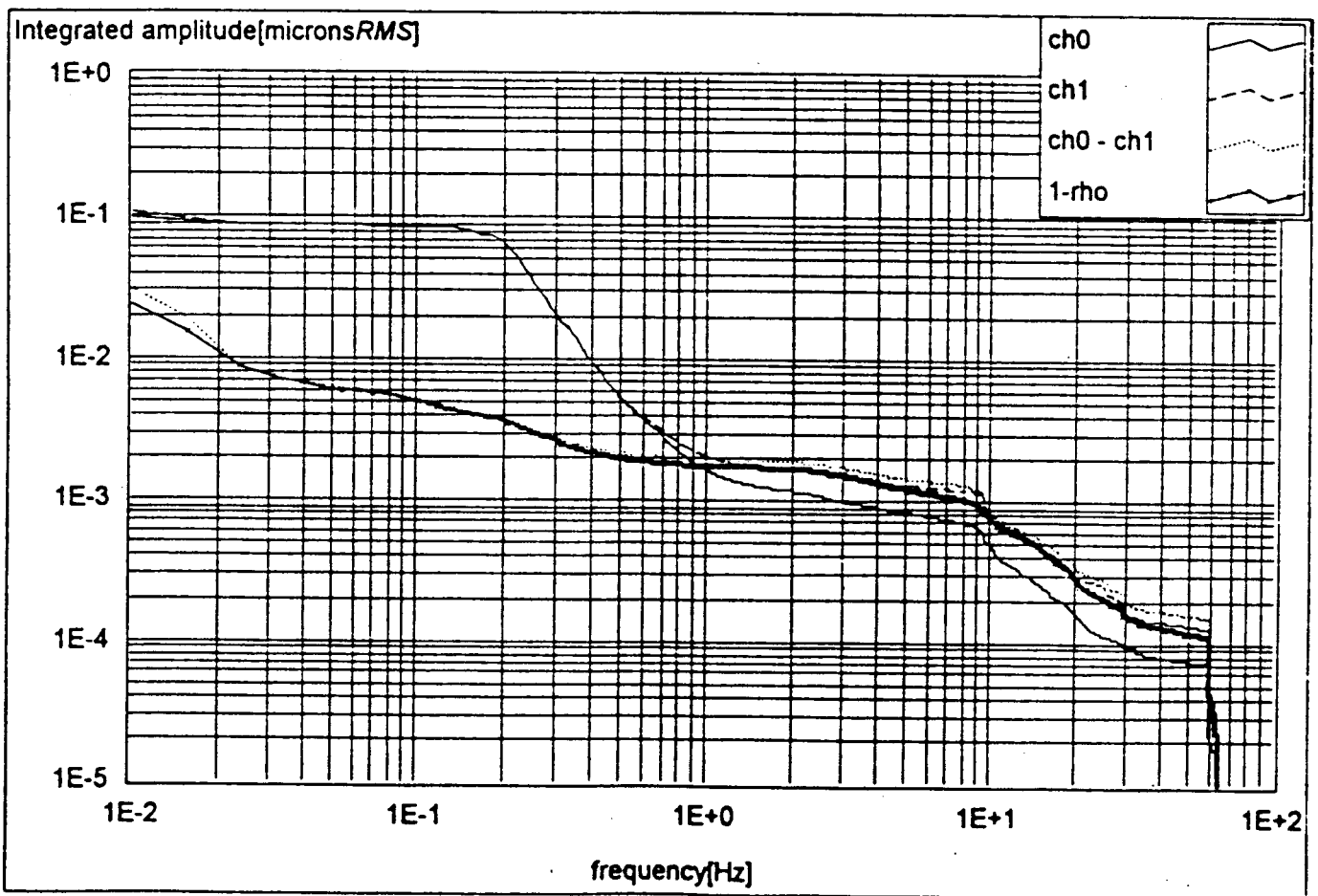
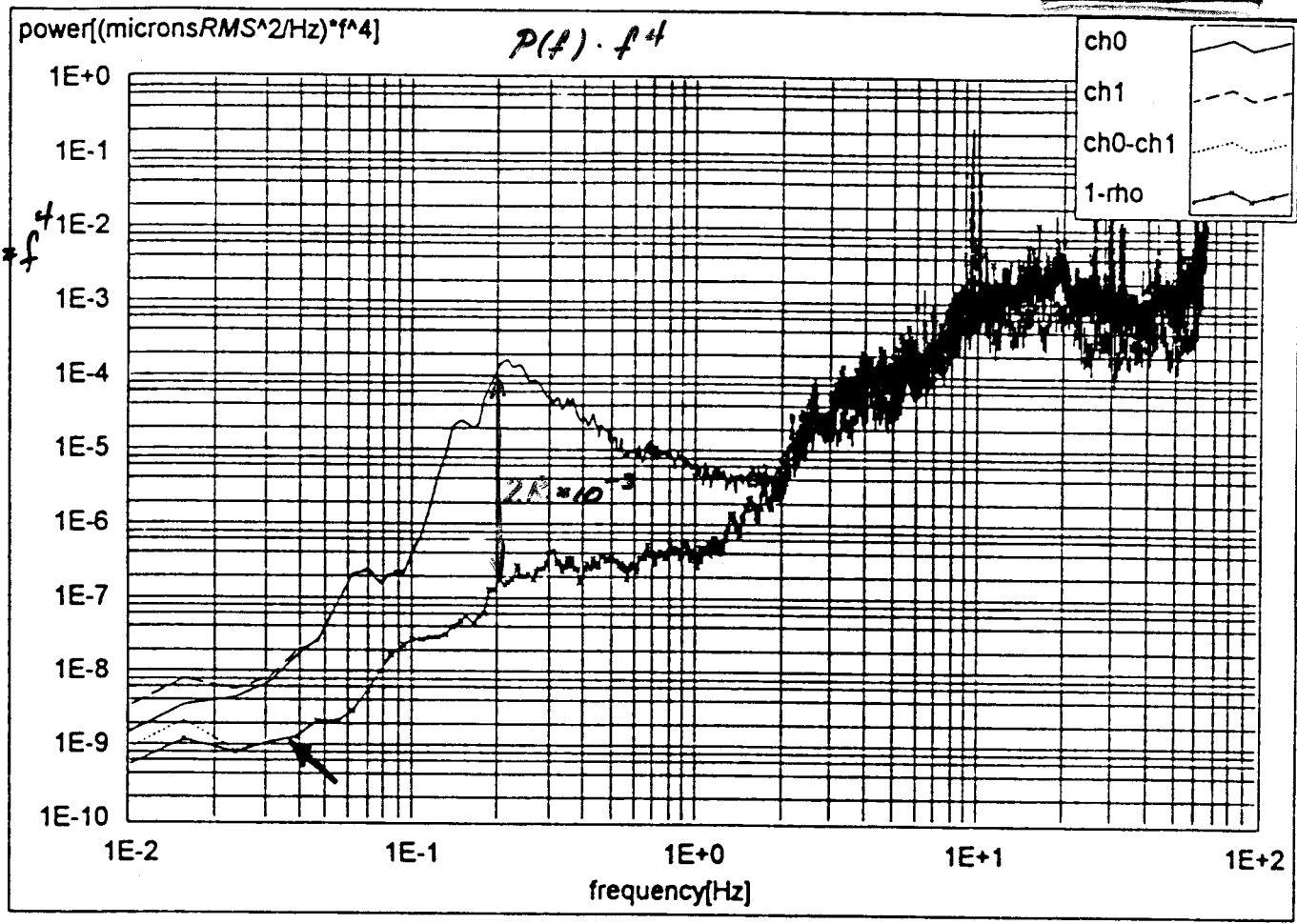
Integrated amplitude[micronsRMS]

ch0
 ch1
 ch0 - ch1
 1-rho

10 $\Delta Z = 100 \text{ m}$

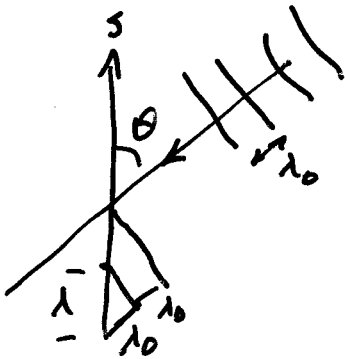
(13)



SUPPOSE "WAVES" OF FREQUENCY ω

had a fixed wavenumber $k_0(\omega) \quad \left[= \frac{\omega}{c(\omega)} \right]$

SUPPOSE THEY WERE ARRIVING FROM ALL DIRECTIONS.



$\frac{d\theta}{(\pi/2)}$ = fraction at angle $d\theta$ { UNIFORM IN θ . "0 to $\pi/2$ "

$$= \frac{2}{\pi} dk \frac{d\theta}{dk}$$

$$\lambda_0 = \lambda \cos \theta$$

$$k = k_0 \cos \theta$$

$$= \frac{2}{\pi} dk \frac{1}{k_0 \sin \theta}$$

fraction in interval dk .

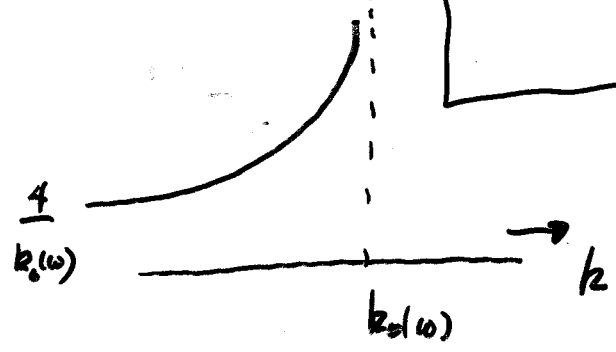
$$\left| \frac{dk}{d\theta} \right| = + k_0 \sin \theta$$

$$= \frac{2}{\pi} \frac{dk}{\sqrt{k_0^2(\omega) - k^2}}$$

$$= k_0 \sqrt{1 - \cos^2 \theta}$$

$$= \sqrt{k_0^2 - k^2}$$

$$\mu(\omega, k) = \frac{4}{\sqrt{k_0^2(\omega) - k^2}}$$



SUPPOSE WE HAVE WAVES - AT ω .

$$\mu(\omega, k) = \frac{4}{\sqrt{k_0(\omega)^2 - k^2}}$$

$$R(\omega, l) = \int \mu(\omega, k) [1 - \cos kl] \frac{dk}{2\pi}$$

$$= 1 - J_0 [k_0(\omega) \cdot l]$$

also $\Rightarrow \frac{k_0^2 l^2}{4}$ as $l \rightarrow 0$

VERY SPECIAL PARTICULAR

SUPPOSE ONLY

$$\overline{k^2}(\omega) \equiv \int k^2 \mu(\omega, k) \frac{dk}{2\pi} < \infty$$

then as $l \rightarrow 0$

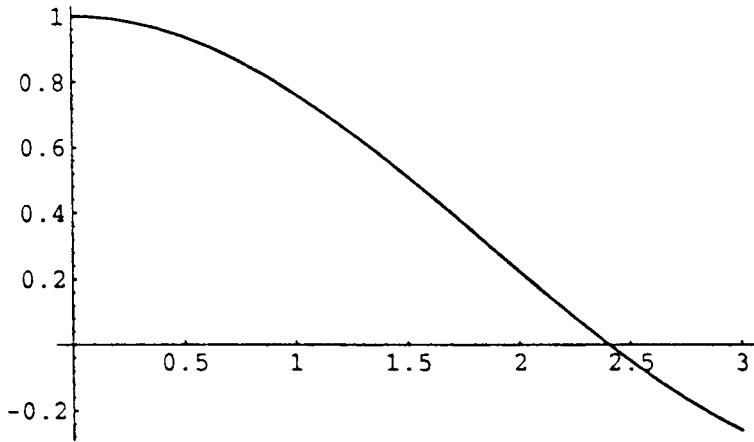
$$R(\omega, l) = \int_0^\infty \mu(\omega, k) [1 - \cos kl] \frac{dk}{2\pi} \rightarrow \frac{1}{2} \overline{k^2}(\omega) \cdot l^2$$

$\approx \frac{1}{2} k^2 l^2$

ALSO QUITE SPECIAL for $k_{mc} l \ll 1$!

[$l \rightarrow 0$ mean $l \ll \lambda$ content of μ ! $kl \ll 1$ typ. k of μ !]

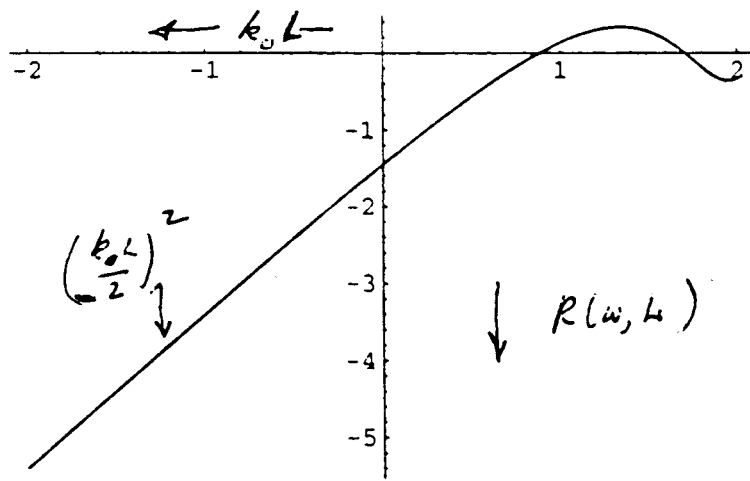
Plot[BesselJ[0,s],{s,0,3}]



"Uniform wave assumption"

-Graphics-

Plot[Log[1-BesselJ[0,Exp[t]]],{t,-2,2}]



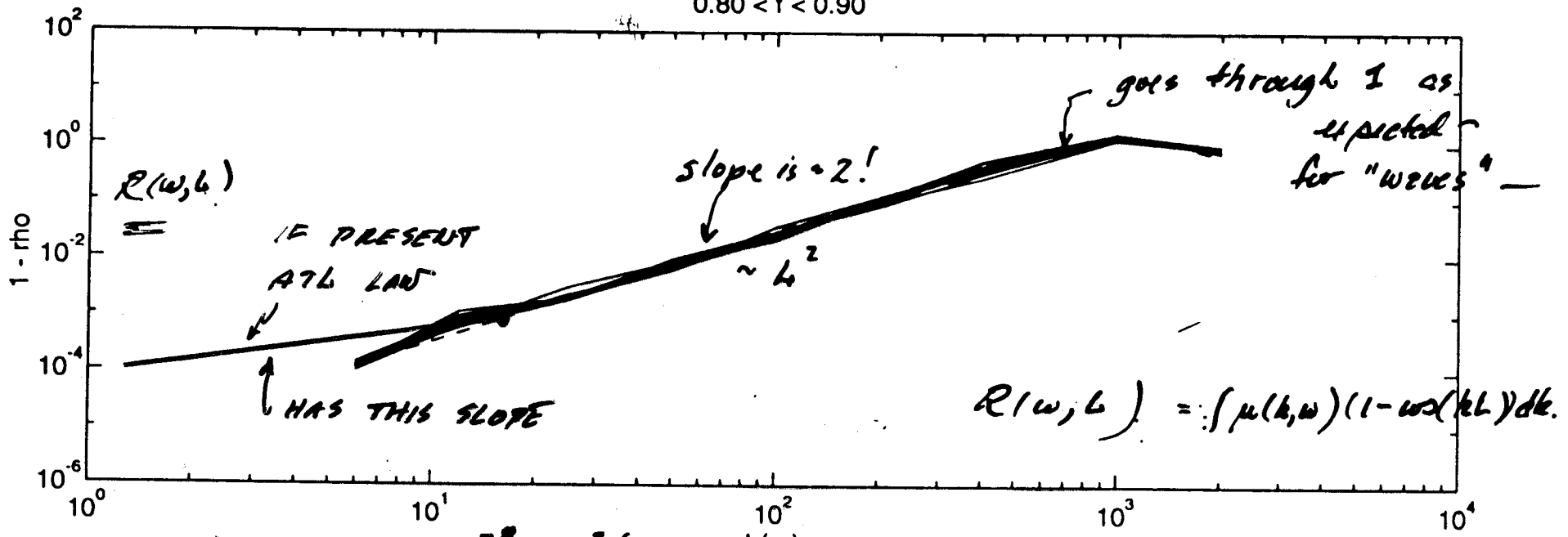
(23)

"k_0 can depend on frequency"

-Graphics-

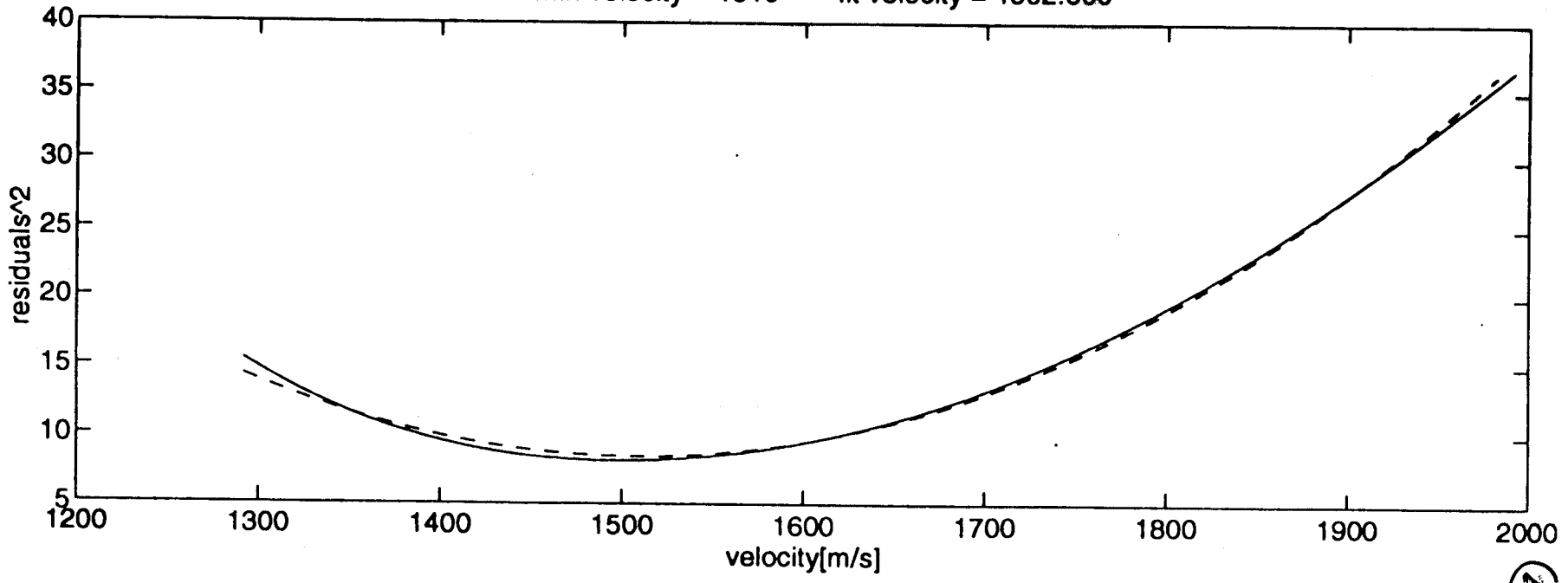
$$J_0(k_0 L) = \int_0^{k_0} \frac{dk}{2\pi} \underbrace{\left(\frac{2\pi}{2\pi} \right) \left(\frac{2}{\pi} \right)}_{\mu(k, \omega)} \frac{4}{\sqrt{k_0^2 - k^2}} \cdot \cos kL$$

0.80 < f < 0.90

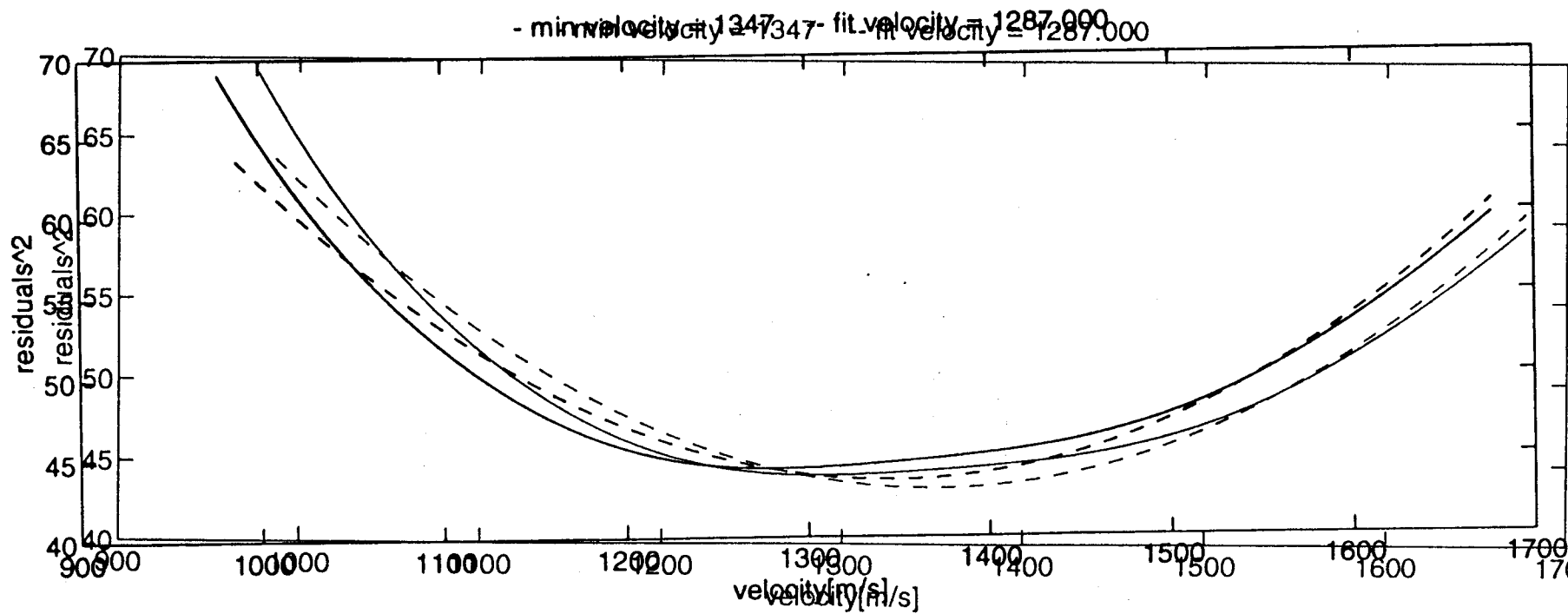
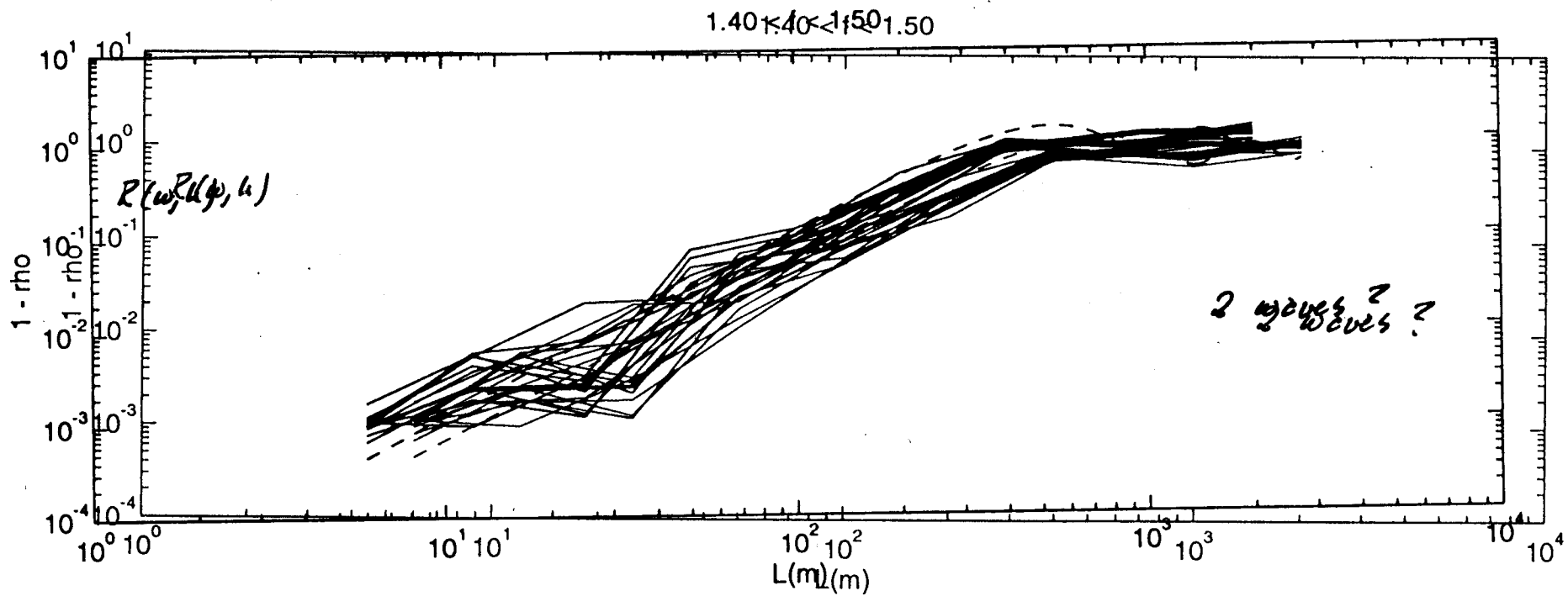


GIVES A S $10^{-8} \text{ mm}^2/\text{m}\cdot\text{s}$
AT $L = 12 \text{ m}$.

- min velocity = 1510 -- fit velocity = 1502.000



14
164

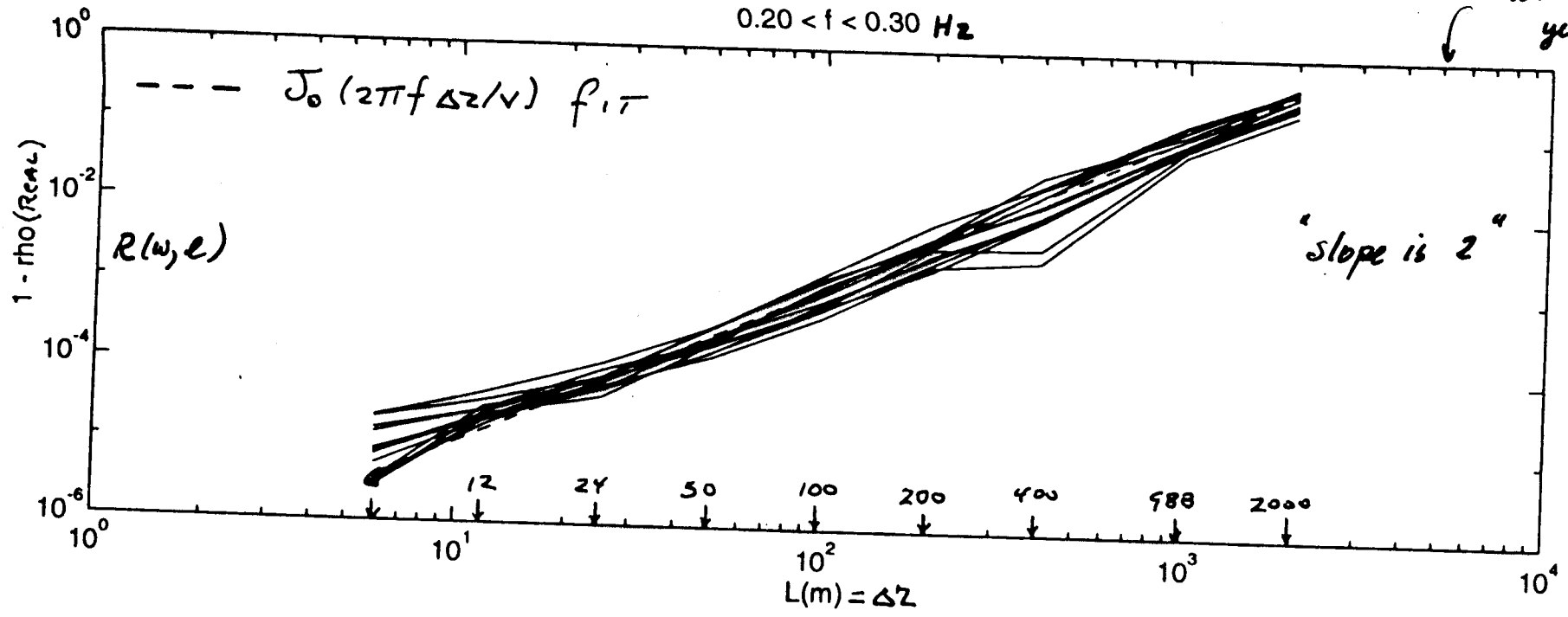


15
(26)

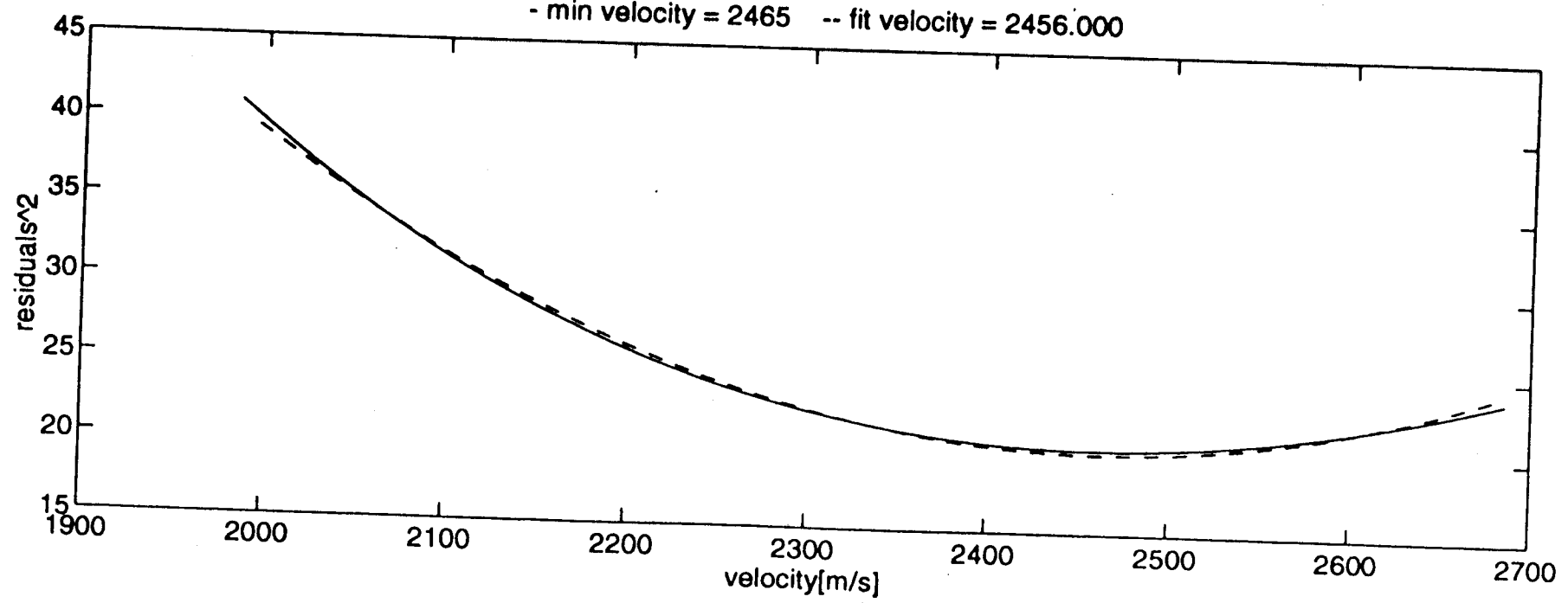
$R(\omega, \ell)$ vs. ℓ .

$0.20 < f < 0.30$ Hz

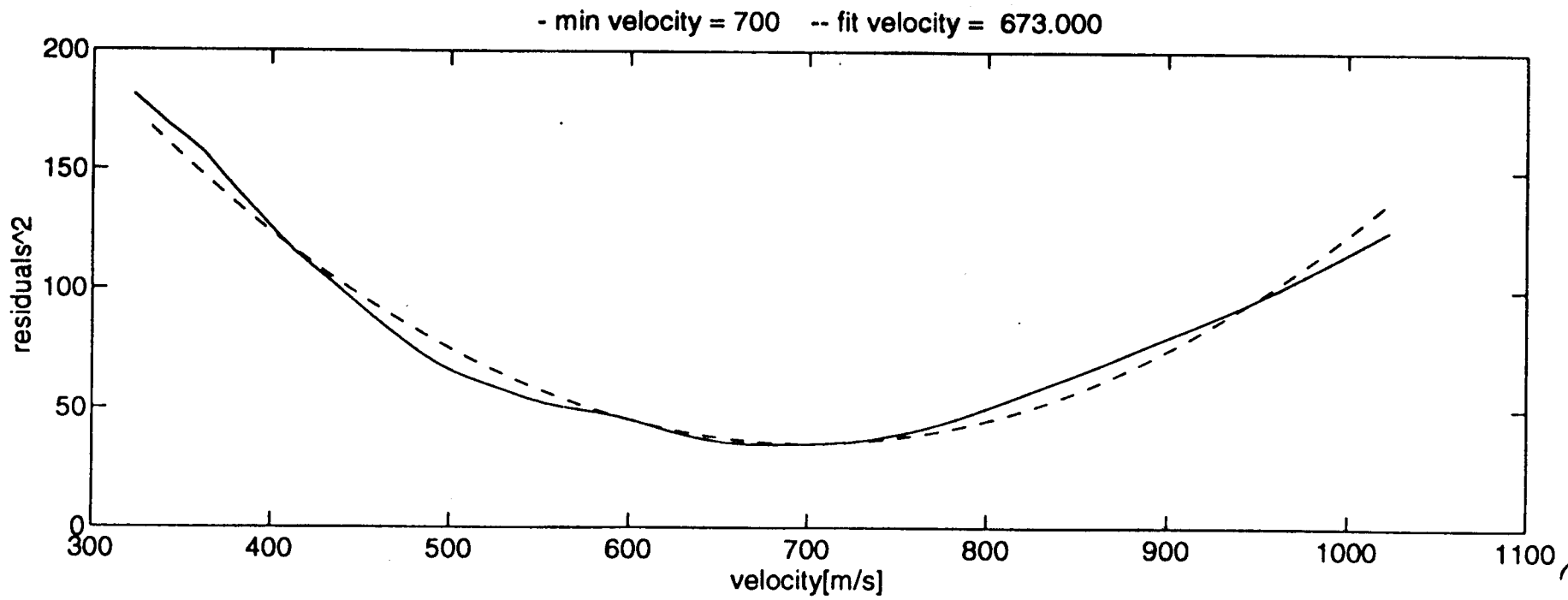
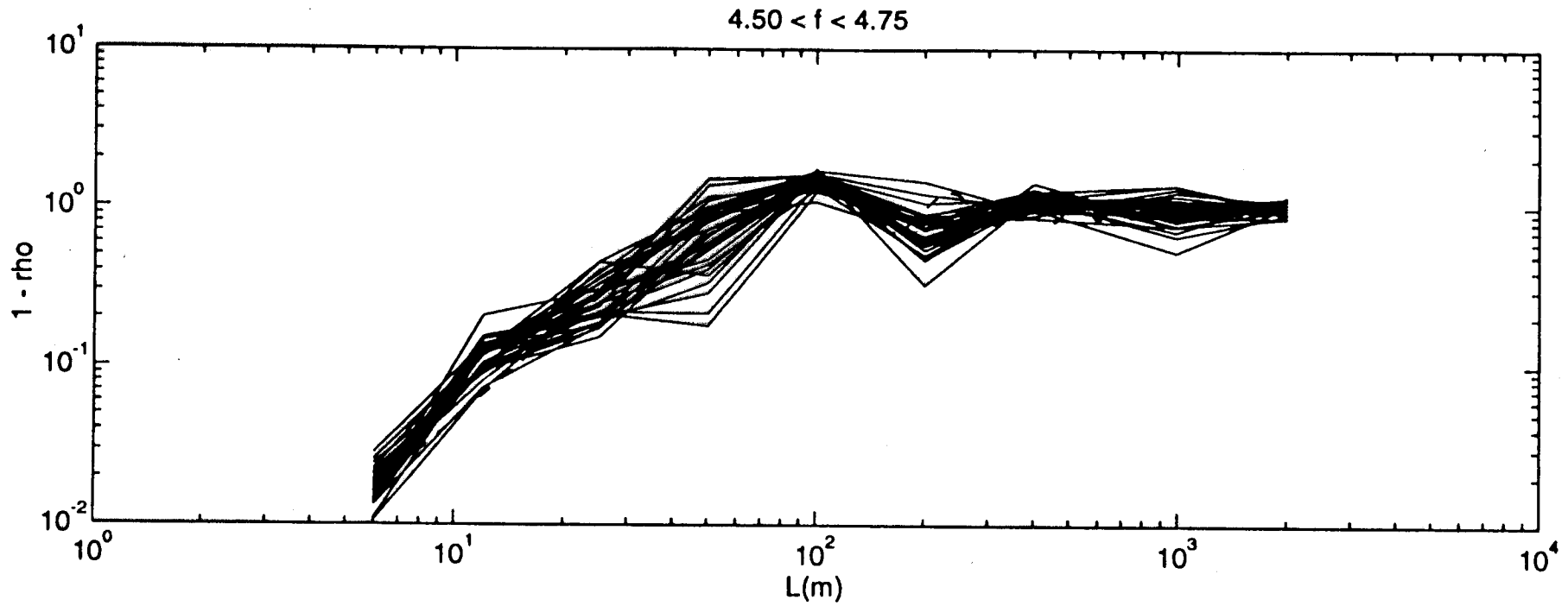
not to 1 yet.



- min velocity = 2465 -- fit velocity = 2456.000



16
24



17
(27)

REMARKS ON ATL LAW.

ATL Law implies

$$\mu(\omega, k) = \mu_R(\omega, k) + \mu_T(\omega, k)$$

with $\mu_T(\omega, k) \rightarrow \frac{A}{k^2 \omega^2}$ as $k \rightarrow \infty$

For $\mu_T(\omega, k)$ $\int k^2 \mu_T(k, \omega) dk \rightarrow \infty$.

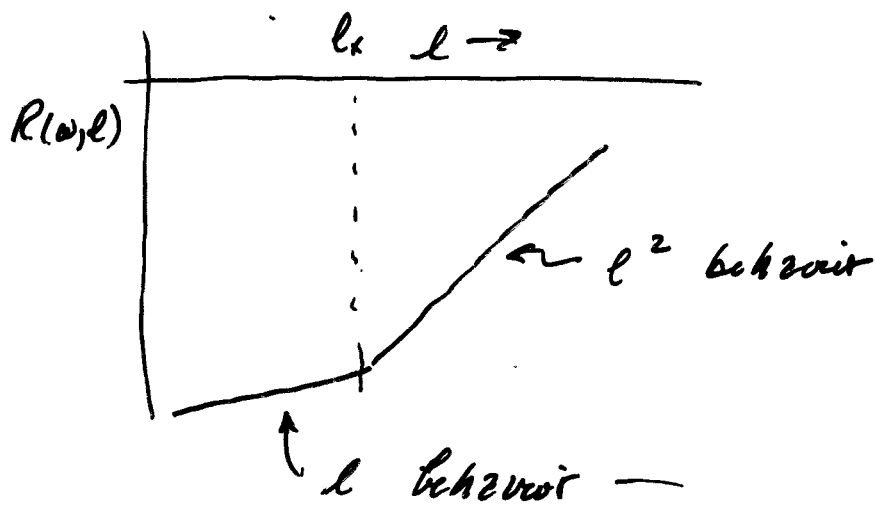
so l^2 behavior not implied —

$$\begin{aligned} R(\omega, l) &\sim \int \frac{1}{k^2} (1 - \cos kl) \frac{dk}{2\pi} \\ &= 2 \int \frac{\sin^2 \frac{kl}{2}}{k^2} \frac{dk}{2\pi} = \frac{l}{2\pi} \int \frac{\sin^2 x}{x^2} dx \\ &\quad \uparrow \text{exists -} \\ &\quad \text{get } l \text{ behavior!} \end{aligned}$$

IF A T L Law is present -

$$R(\omega, l) \rightarrow \alpha l^2 + \beta l \quad \text{as } l \rightarrow 0$$

at $l_x = \frac{\beta}{\alpha}$ 2 terms are equal.



From $R(\omega, l)$ data can put a limit on β !

$$\Rightarrow A < 0.6 \times 10^{-6} \quad 0.1 < f < 10$$

[SERV & NAPOLY ASSUME $A = 10^{-4}$ to 10^{-5} .]

LATTICE MOTION

$$G(k) \equiv \frac{\langle \Delta y_{IP}^2 \rangle(k)}{y_0(k)^2} \quad \text{plane wave response}$$

- avg. over phase -

$$G(k) \sim k^b \text{ as } k \rightarrow 0 \quad \text{FOR "PAIRED" LATTICES}$$

$$G_\mu(\omega) = \int G(k) \mu(\omega, k) \frac{dk}{2\pi}$$

$$F(\omega) \equiv \text{POWER SUPPRESSION FROM FEEDBACK SYSTEM}$$

$$\begin{aligned} \langle \Delta y_{IP}^2 \rangle &= \int P(\omega, k) G(k) F(\omega) \frac{dk}{2\pi} \frac{d\omega}{2\pi} \\ &= \int P(\omega) G_\mu(\omega) F(\omega) \frac{d\omega}{2\pi} \end{aligned}$$

- THE LITTLE RESPONSE FUNCTION -

$$\Delta y_B(t) \equiv y_B(t) - y(t, 0)$$

$$= \int_0^L K(s) y(t, s) R_{34}(s) ds + R_{33}(L) y(t, L) - y(t, 0)$$

$$= \sum_i \mu_i y(t, s_i) \quad (\text{slices})$$

$$\langle \Delta y_B(t)^2 \rangle_t = \sum_{i,j} \mu_i \mu_j \langle y(t, s_i) y(t, s_j) \rangle_t$$

$$= \sum_{i,j} \mu_i \mu_j \int_0^\infty P(k) \cos[k(s_i - s_j)] \frac{dk}{2\pi}$$

$$= \int_0^\infty P(k) \underbrace{\sum_{i,j} \mu_i \mu_j \cos[k(s_i - s_j)]}_{G(k)} \frac{dk}{2\pi}$$

$$G(k) \equiv \sum_i \mu_i \mu_j (\cos k s_i \cos k s_j + \sin k s_i \sin k s_j)$$

$$\boxed{G(k) = \left(\sum_i \mu_i \cos k s_i \right)^2 + \left(\sum_i \mu_i \sin k s_i \right)^2}$$

$$= \int_0^\infty P(k) G(k) \frac{dk}{2\pi}$$

Δy^2 response to sin wave, $\lambda = \frac{2\pi}{k}$.

FOR TWO FINAL FOCUS SYSTEMS.

$$\sum \mu_i \cos k s_i = 0 \quad \text{by symmetry}$$

HENCE

$$G(k) = 4 \left(\sum_i \mu_i \sin k s_i \right)^2$$

one
side

"SUM RULES"

note:

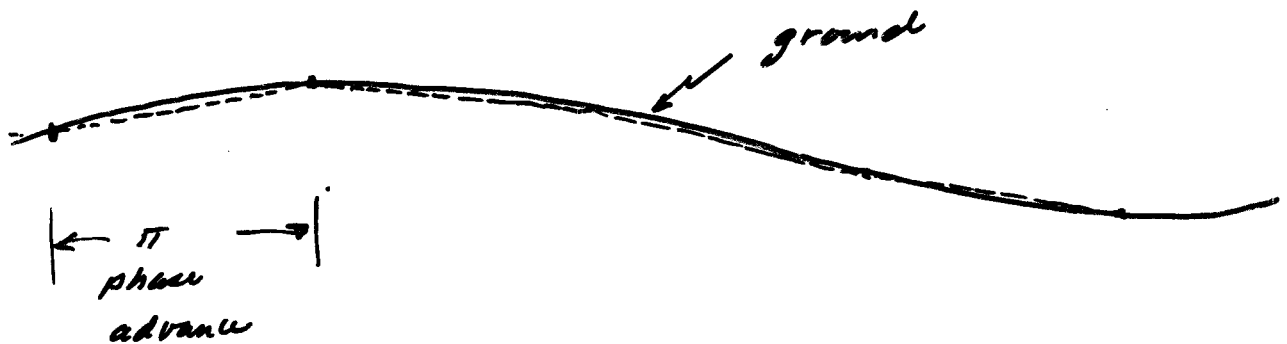
$$\sum \mu_i s_i = 0$$

so

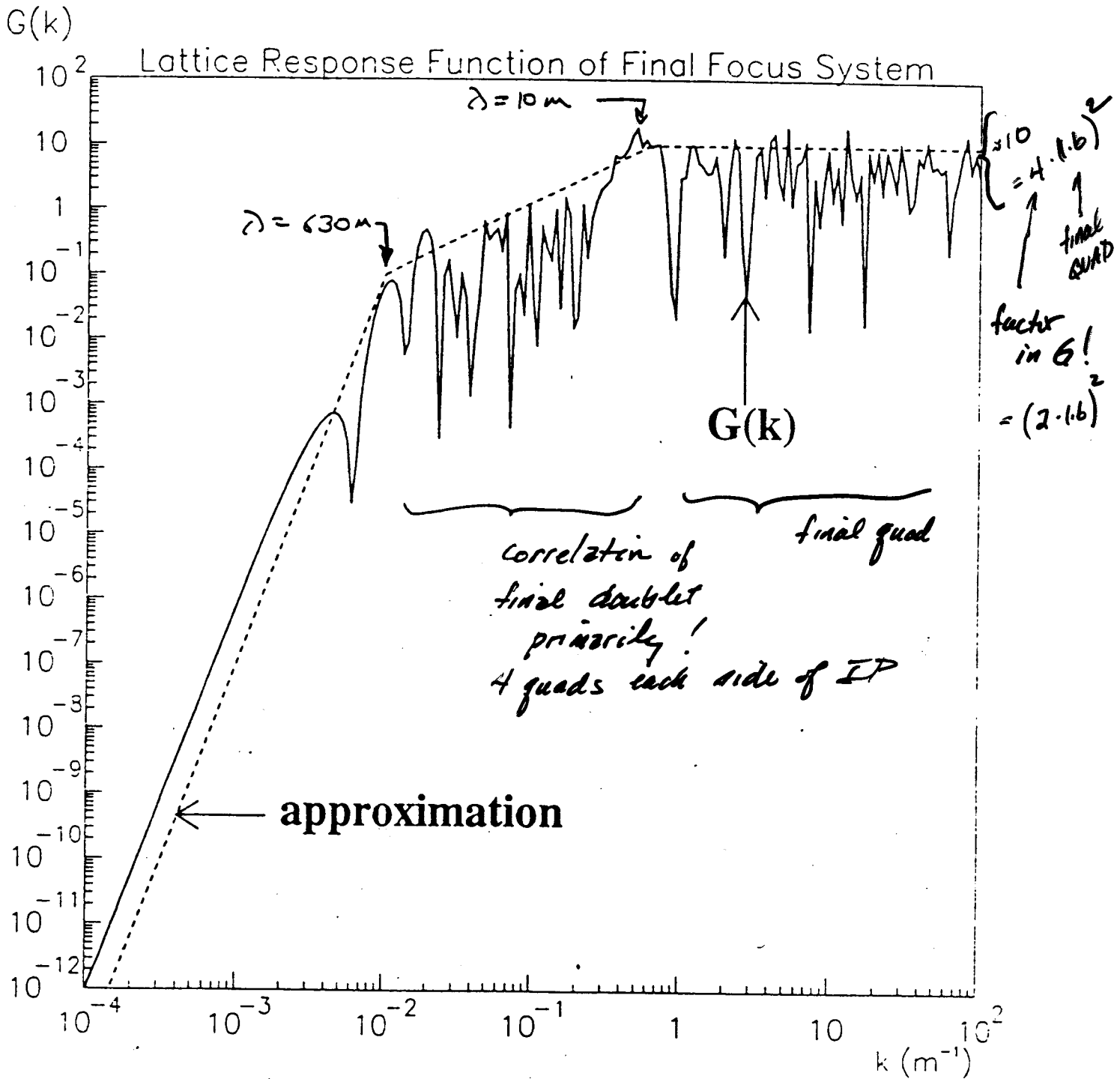
$$G(k) \sim k^4 \quad k \rightarrow 0$$

but in a paired lattice

$$G(k) \sim k^6 !$$



for straight line approx —
 $\Delta y_B = 0 !$



$\frac{1}{4} = \frac{630}{4} \approx 160 \text{ m}$ is length
of π sections in FF system.

Zimmerman

TO GET A SPECIAL DECOMPOSITION OF $\langle Ay_B(t)^2 \rangle$?

$$\langle Ay_B(t)^2 \rangle_t = \int_0^\infty P(\omega, k) G(k) \frac{dk}{2\pi} \frac{d\omega}{d\omega}$$

$$= \int_0^\infty P(\omega) \underbrace{\int_0^\infty \mu(\omega, k) G(k) \frac{dk}{2\pi}}_{\equiv G_\mu(\omega)} \cdot \frac{d\omega}{2\pi}$$

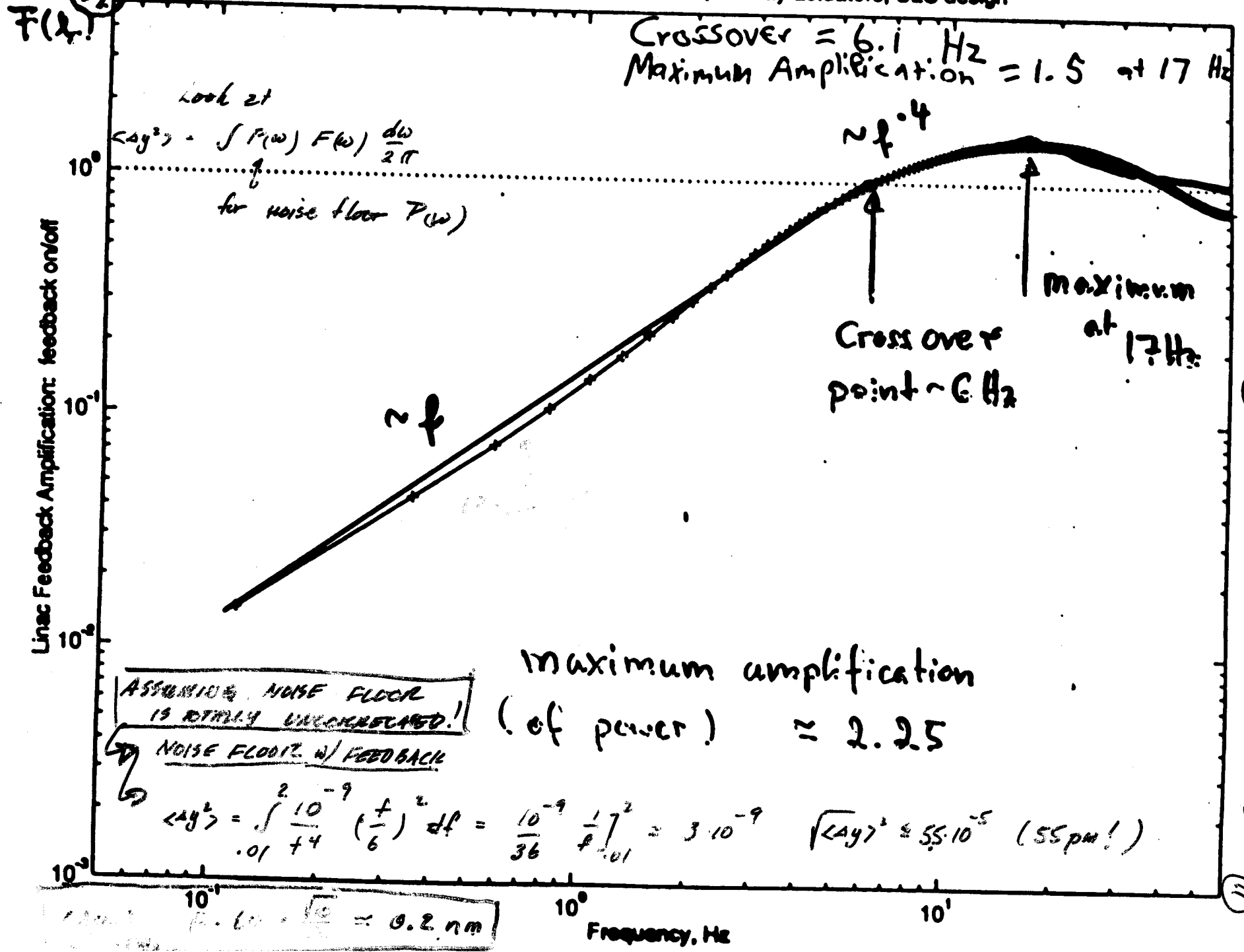
$$= \int_0^\infty P(\omega) G_\mu(\omega) \frac{d\omega}{2\pi}$$

If there is suppression of low freq. by a feedback system.

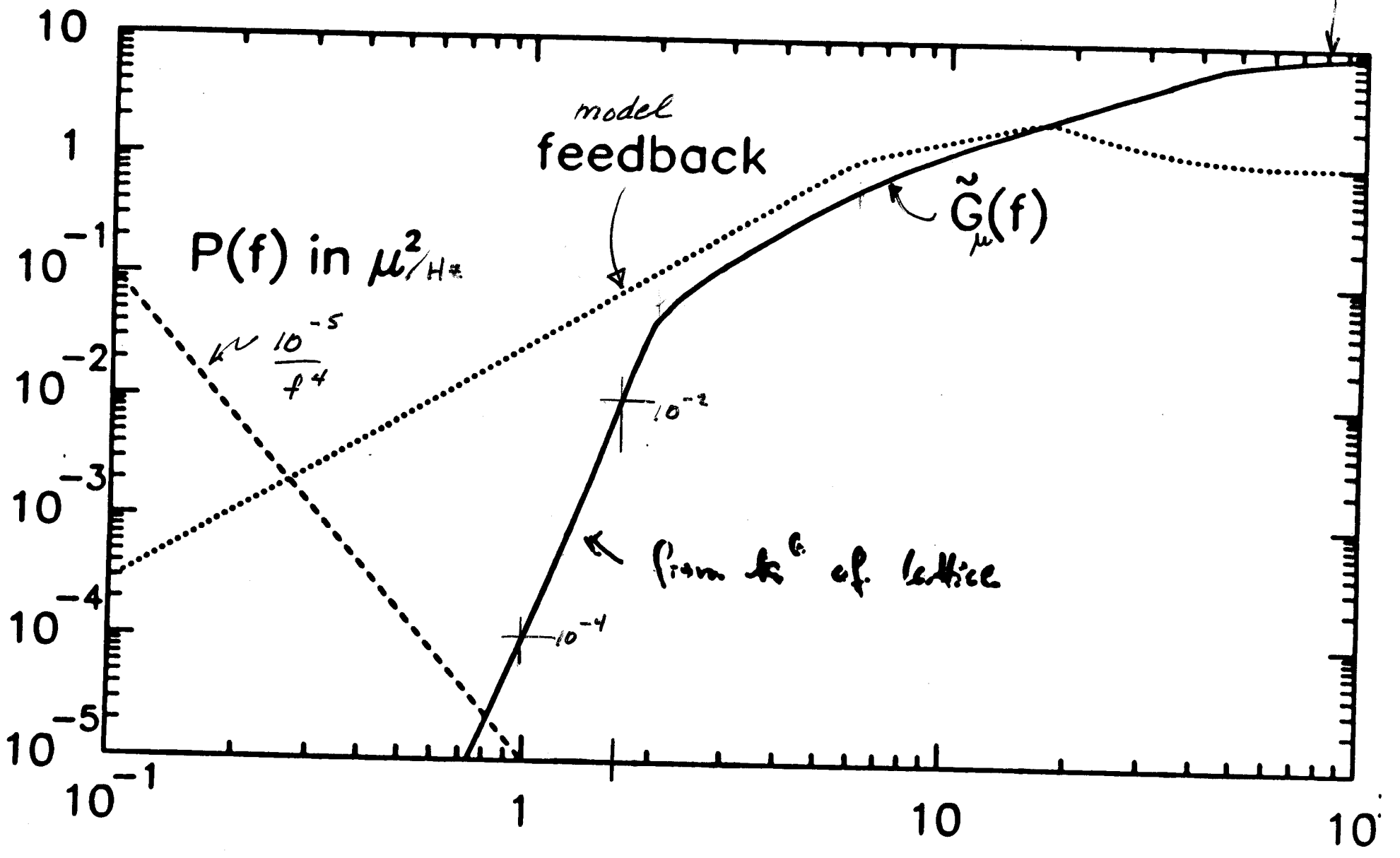
$$\langle Ay_B(t)^2 \rangle_t = \int_0^\infty P(\omega) G_\mu(\omega) F(\omega) \frac{d\omega}{2\pi}$$

5. NLC Feedback with imperfect cascade (Linde Hendrickson)

NLC: imperfect cascade simulation, 2 delay actuators, SLC design

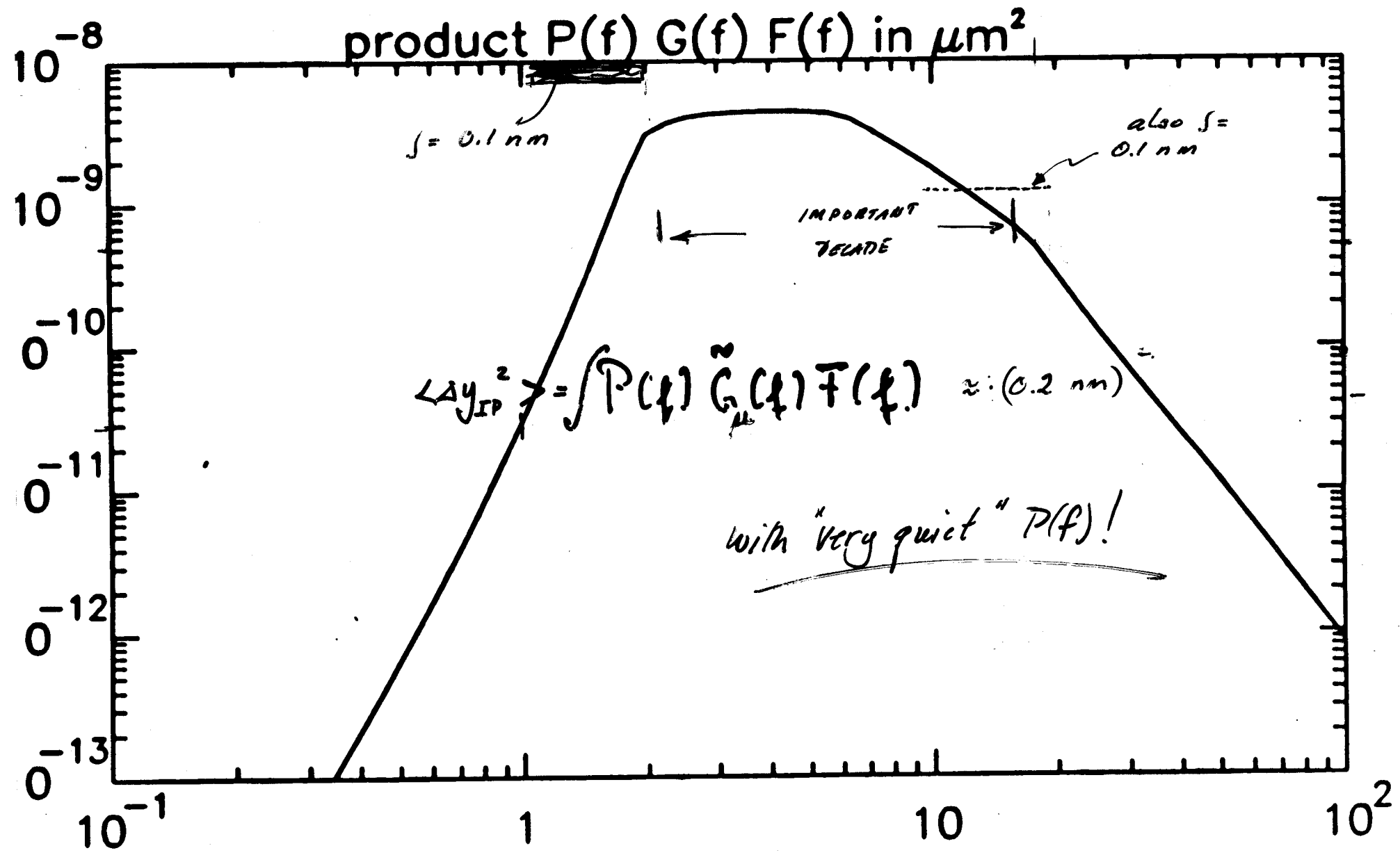


C.I. 11



multiply these 3 functions

f (Hz)

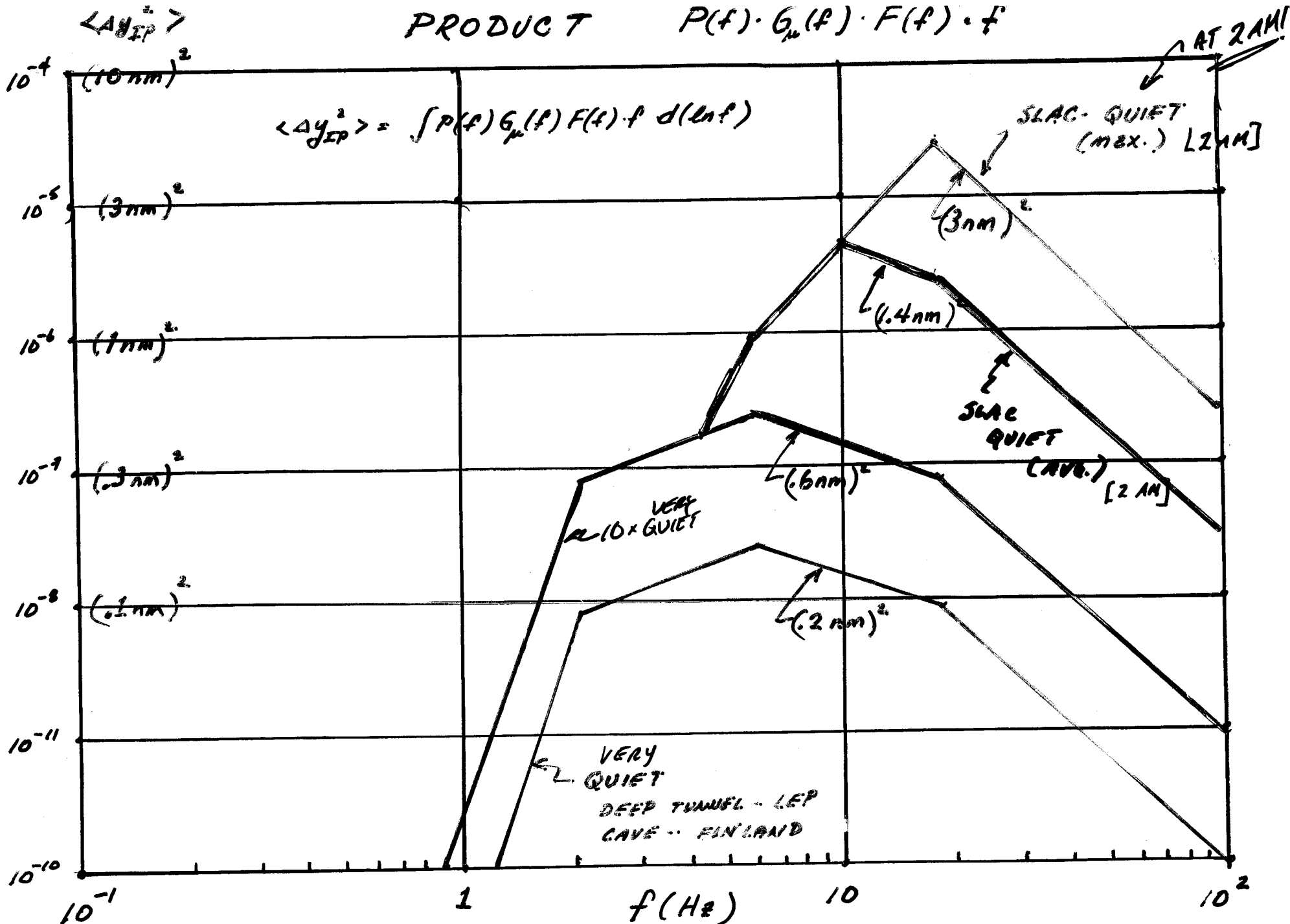


... and integrate over f ...

$$G_{\mu}(f) = \int G(k) \mu(\omega, k) \frac{dk}{2\pi}$$

Zimmerman

PRODUCT $P(f) \cdot G_{\mu}(f) \cdot F(f) \cdot f$



$$\frac{\Delta L}{L} = \frac{1}{16} \frac{\langle \Delta y_{EP}^2 \rangle}{\sigma_y^2}$$

← 4 ——— IMPORTANT DECADE ——— → 10
 IMPORTANT @ QUADS

MY FAVORITE STRATEGY FOR IP REGIONS

[ASSUMING FINAL QUADS INSIDE DETECTOR]

I. RESONANCES

FINAL QUADS IN A "TUBE"

→ SYSTEM HAS RESONANT FREQUENCIES

TIME OF GROWTH $\tau_{\text{damp}} \gg \frac{2\pi}{\omega_n}$

→ STEERING (DEFLECTION!) BY OFFSET BEAMS
IS VERY STRONG & EASILY MEASURABLE

FILTER FOR RESONANT MODES

→ STEER BEAM TO NULL SIGNAL —
(at ω_n 's)

PRESUMABLY THIS TAKES CARE OF
VIBRATION SOURCES WITHIN DETECTOR —

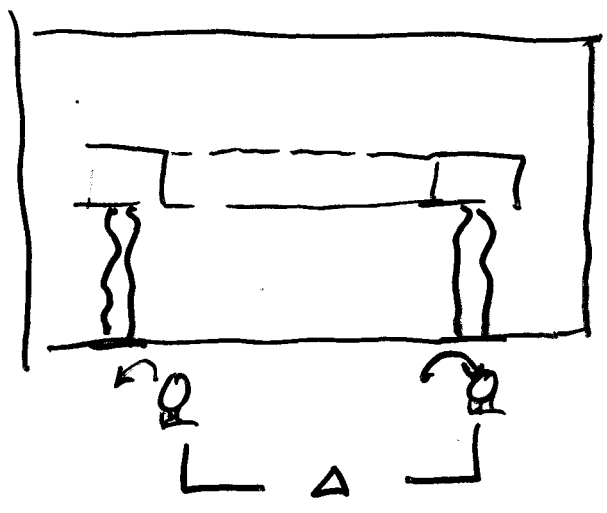
II. ANTI-SYMMETRIC "BEAM" MOTIONS

- NON-RESONANT -

PRESUMABLY DUE TO GROUND MOTION

- MEASURE ^{ANTI-SYMMETRIC} GROUND MOTION AT "SOURCE"

- BASE OF DETECTOR -



- DEDUCE ^{SUPPORT} BEAM (NON-RESONANT) MOTION

- MODEL
 - MEASUREMENTS } ADAPTIVE PARAMETERS

- COMPENSATE w/ BEAM STEERING

EXTERNAL QUADS NEAR IP... LIKEWISE

CONCLUSIONS

- 1.) $P(\omega)$ VARIES A LOT -
 - DEEP TUNNELS DRAMATICALLY BETTER IN CRUCIAL REGIONS -
 - & LESS SUSCEPTIBLE TO CHANGES IN "CULTURAL" BACKGROUNDS

- 2.) $\mu(\omega, k)$ MAY BE CONSTANT - CHECKS?

- 3.) $\mu(\omega, k)$ WELL-FIT W/ UNIFORM WAVES AT SOME $\nu(\omega)$. CHECKS

- 4.) LIMITS CAN BE PLAYED ON ATL COEFF IN HIS FREQ. RANGE -

- 5.) AT DEEP - VERY QUIET SITES - ~
 GROUND MOTION $\langle a_{g,IP}^2 \rangle \sim (0.2 \text{ nm})^2$
 IS ACCEPTABLE
 A SURFACE SITES - NOT ACCEPTABLE
 W/O FURTHER INTERVENTION!