

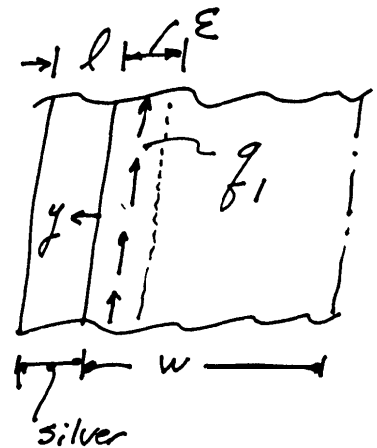
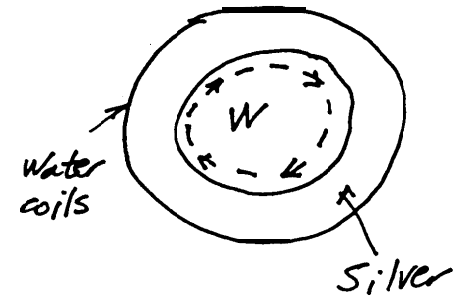
# FORMULATION

①

## TWO SOLUTIONS SUPERIMPOSE (LINEAR EQUATIONS):

$T_1$  = FIRST IS FOR A CONTINUOUS ANNULUS OF HEATING ACROSS PATH WIDTH  $\epsilon$  (ABOUT 4.4 KW).

$T_2$  = SECOND IS FOR AN INDIVIDUAL PULSE MOVING AT VELOCITY  $u$  AND HAVING PULSE STRENGTH  $Q_p$



$$T_1 = T_1(y) \quad \frac{d^2 T_1}{dy^2} = \begin{cases} 0, & y < -\epsilon \\ q_1/k_w, & -\epsilon < y < 0 \\ 0, & 0 < y < l \end{cases}$$

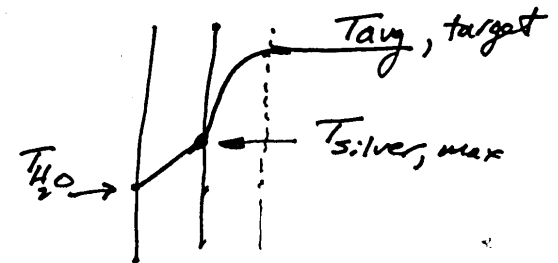
obtain: for  $-\epsilon < y < 0$ :

$$T_1 = T_{\text{avg, target}} + \frac{q_1}{2k_w} (\epsilon^2 - y^2) - \frac{q_1}{k_w} \epsilon (y + \epsilon)$$

$0 < y < l$ :

$$T_1 = T_{\text{avg, target}} + \frac{q_1 \epsilon y}{k_{\text{silver}}} - \frac{q_1 \epsilon^2}{2k_w}$$

Set  $T_1 \approx T_{H_2O}$  to obtain  $T_{\text{avg, target}}$  for  $y=l$



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$$q_i = \frac{Q_{TOTAL}}{\pi D_o \cdot 2\epsilon \cdot z} = \frac{4.4 \text{ kW} \times 3,413 \frac{\text{Btu}}{\text{kWh}}}{\pi \left(\frac{2.5}{12}\right) \left(\frac{0.12}{30.48}\right) \frac{0.4}{12} \text{ ft}^3} = 1.7 \times 10^8 \frac{\text{Btu}}{\text{ft}^3} \quad (2)$$

$$\epsilon \approx \frac{0.12}{30.48} = 0.004 \text{ ft} \quad ; \quad l = 0.10 \text{ mil} = 0.0083 \text{ ft}$$

$$h_{kw} = 95 \frac{\text{Btu}}{\text{ft}^2 \cdot \text{hr} \cdot \text{F}} \quad ; \quad h_{silver} \approx 200 \frac{\text{Btu}}{\text{ft}^2 \cdot \text{hr} \cdot \text{F}} \quad ; \quad T_{H_2O} \approx 60^\circ \text{F}$$

$$T_{avg, target} = T_{H_2O} + \frac{q_i \epsilon^2}{2 h_{kw}} + \frac{q_i \epsilon l}{h_{silver}}$$

$$= 60 + \frac{(1.7 \times 10^8)(0.004)^2}{2(95)} + \frac{(1.7 \times 10^8)(0.004)(0.0083)}{200}$$

$$= 60 + 14 + 28 = 102^\circ \text{F} = 39^\circ \text{C} \quad \text{too low}$$

$T_2 = T_2(y, x)$  for an individual, moving pulse

(3)

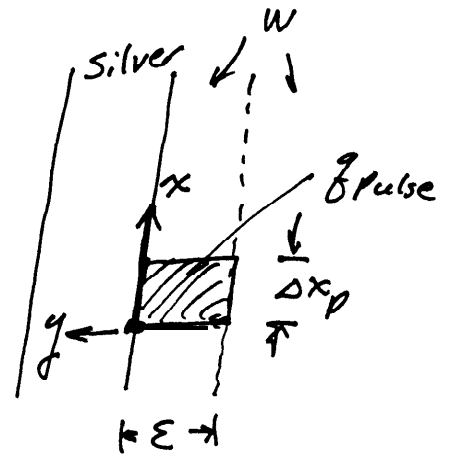
$-\varepsilon < y < 0$ :

$$(1) \quad \frac{\partial^2 T_2}{\partial x^2} + \frac{u}{\alpha_w} \frac{\partial T_2}{\partial x} + \frac{\partial^2 T_2}{\partial y^2} = \begin{cases} 0, & -\infty < x < 0 \\ -\frac{q_{\text{pulse}}}{k_w}, & 0 < x < \Delta x_p \\ 0, & x > \Delta x_p \end{cases}$$

$0 < y < l$ :

$$(2) \quad \frac{\partial^2 T_2}{\partial x^2} + \frac{u}{\alpha_{\text{silver}}} \frac{\partial T_2}{\partial x} + \frac{\partial^2 T_2}{\partial y^2} = 0$$

Subject to:  $\frac{\partial T_2}{\partial y} = 0$  on  $y = -\varepsilon$   
 $T_2 = 0$  on  $y = l$



Coordinates are fixed on heating spot, target travels under at  $u$

because boundary conditions for  $T_1$  and  $T_2$  must also superpose.

The complete solution is then  $T_1 + T_2$ , so cooling coil fluxes are additive

- Note that the solution for  $T_1$  need not be performed by numerical means since a closed form solution is available.
- Solution for  $T_2$  to be obtained numerically. Another solution strategy for  $T_2$  is by Fourier transforms.

Fourier transform:

$$V(\omega, y) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{i\omega x} T_2(x, y) dx$$

Inversion  $\Rightarrow$   $T_2(x, y) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{-i\omega x} V(\omega, y) d\omega$

$$\mathcal{F}\left(\frac{\partial V_2}{\partial x}\right) = -i\omega V \quad ; \quad \mathcal{F}\left(\frac{\partial^2 T_2}{\partial x^2}\right) = -\omega^2 V$$

(1) transforms to an ODE:

$$\frac{d^2 V_a}{dy^2} - \omega(\omega + i\frac{\mu}{\alpha_w}) V_a + \frac{i \rho_{pulse}}{\sqrt{2\pi} \omega} (1 - e^{i\omega \alpha_w}) = 0$$

(2) transforms to another:

$$\frac{d^2 V_b}{dy^2} - \omega(\omega + i\frac{\mu}{\alpha_{silver}}) V_b = 0$$

At  $y=0$ :  $k_w \frac{dV_a}{dy} = k_{silver} \frac{dV_b}{dy}$  and  $V_a = V_b$

Do inversion numerically (by integration)

(4)

FEEDBACK ON  $\Delta T$  cooling water

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