

Apparatus of straightness  
measurement with  
tensioned wires.

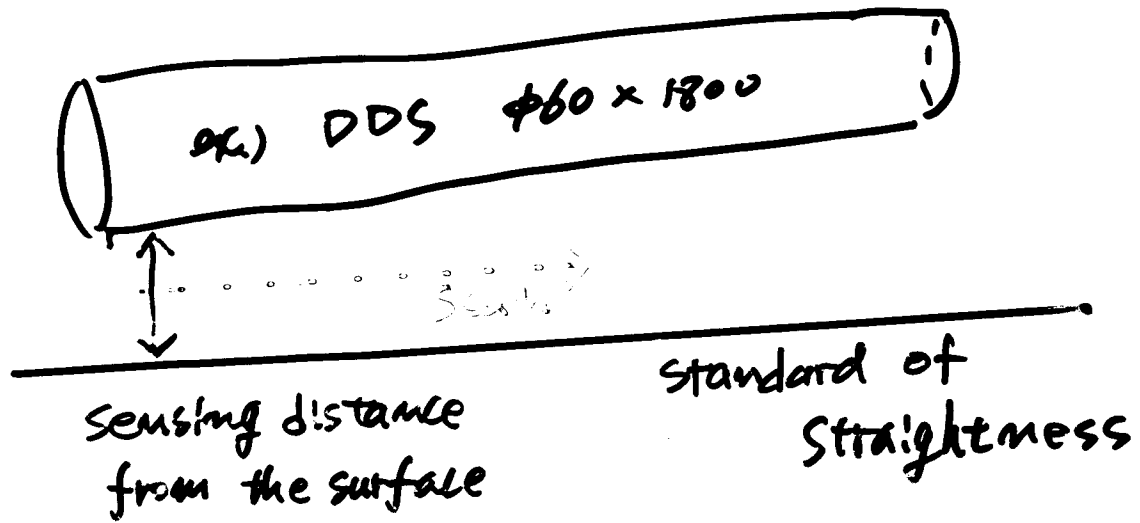
1999. 1. 25

KEK

T. Suzuki

- [1] Current apparatus
- [2] Some ongoing tests

# Methods of straightness measurement



	Sensing	Standard
(1)	Microsense	Linear guide + Laser Interferometer
(2)	Laser Scan Micrometer	Tensioned wires
(3)	multi-Microsense (x2 or x3)	database

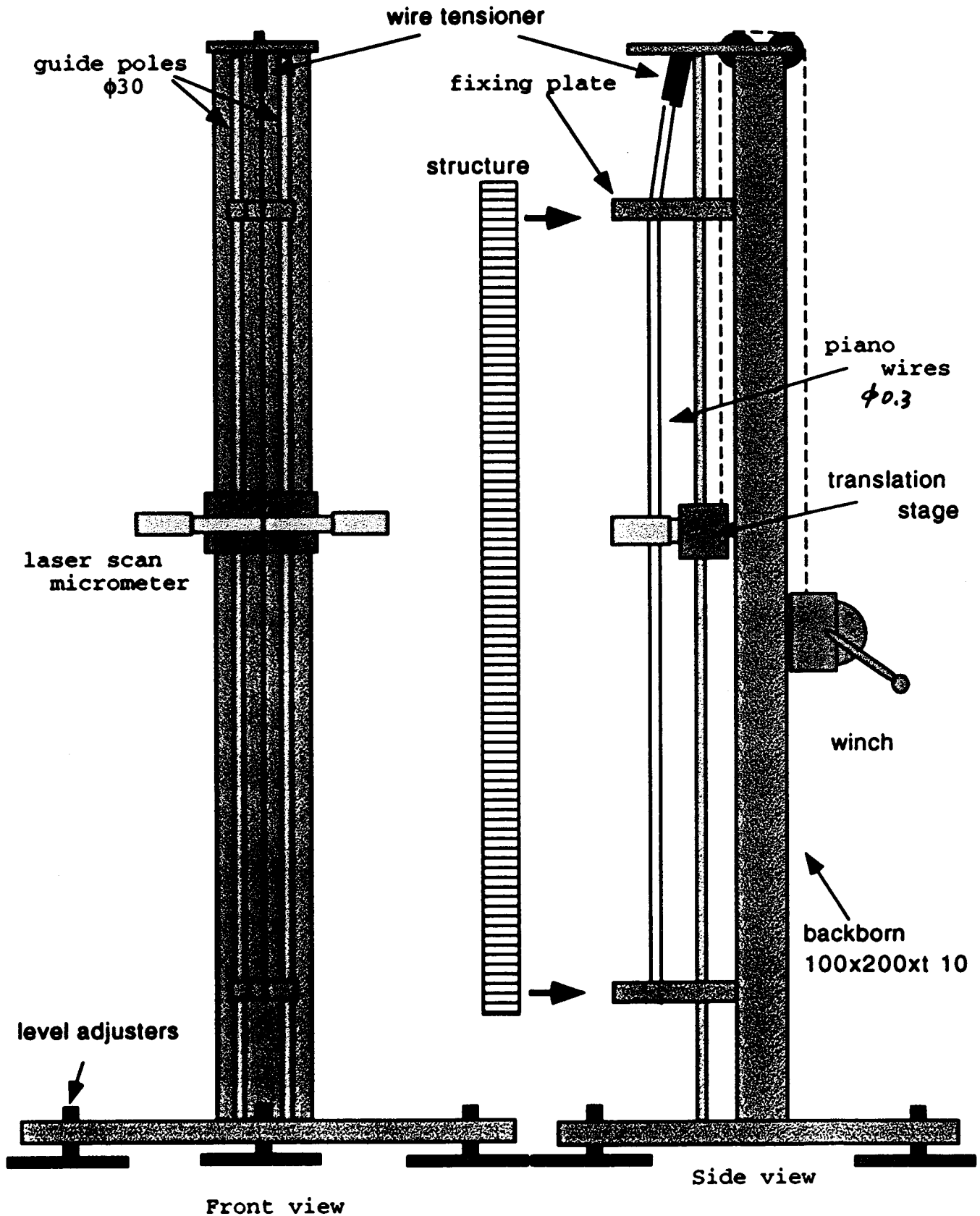
(1): for DDS, stacked disks on v-block  
 $0 \leq \theta \leq 90^\circ$

(2): : , prebonded, d-bonded  
 $\theta = 90^\circ$

(3): under development for LC applications  
Basic experiments have already done.  
(Kiyomo)

# Schematic drawing of <sup>a</sup>straightness measurement

Projection of the structure is compared with a tensioned wire.



## o Wires

$\phi 0.3$  piano wire

tension  $\sim 7$  kgf

measured by the string  
vibration

## o Laser Scan Micrometer

### Specifications

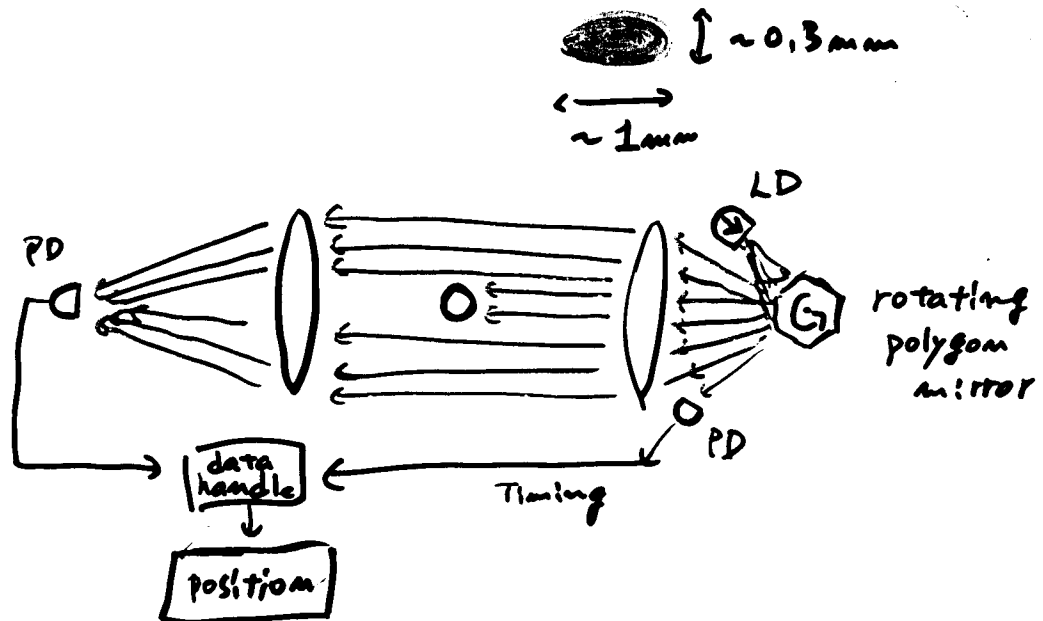
Scan range 40 mm

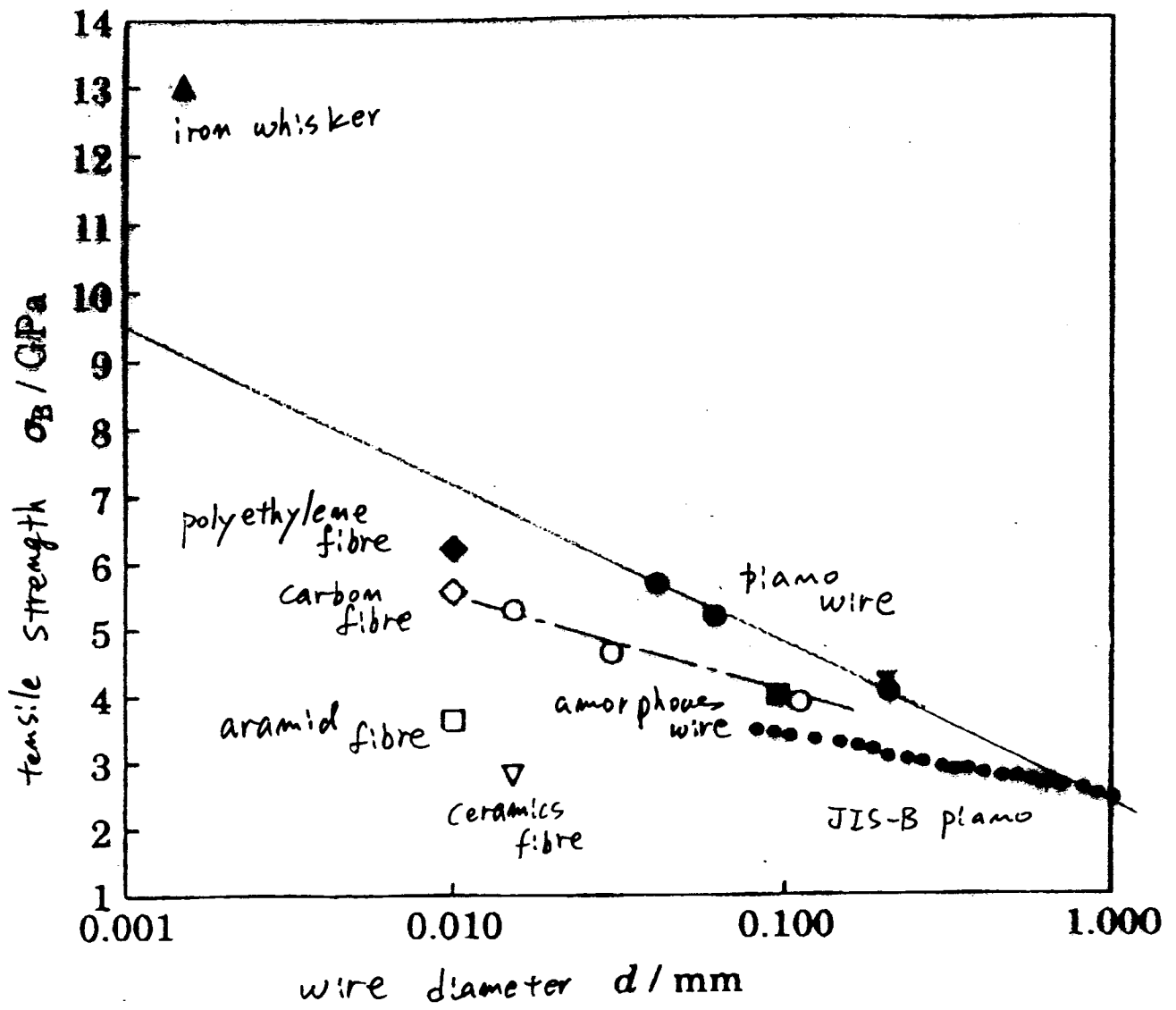
min. detectable  
size 0.2 mm

sensing span  $160 \pm 40$  mm

accuracy  $\pm 2 \mu\text{m}$

Laser 670nm 0.8mW LD





Strength of some  
engineering materials

# Intensity of laser beam on PD

9 Dec. 97

laser beam profile :  $\exp(-y^2/s^2)$

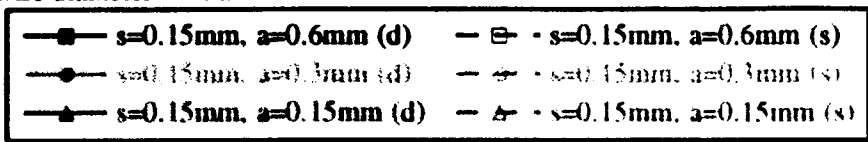
wire position :  $y_0$

wire diameter :  $a$

laser wavelength :  $1\mu\text{m}$

focal length of the lens : 100mm

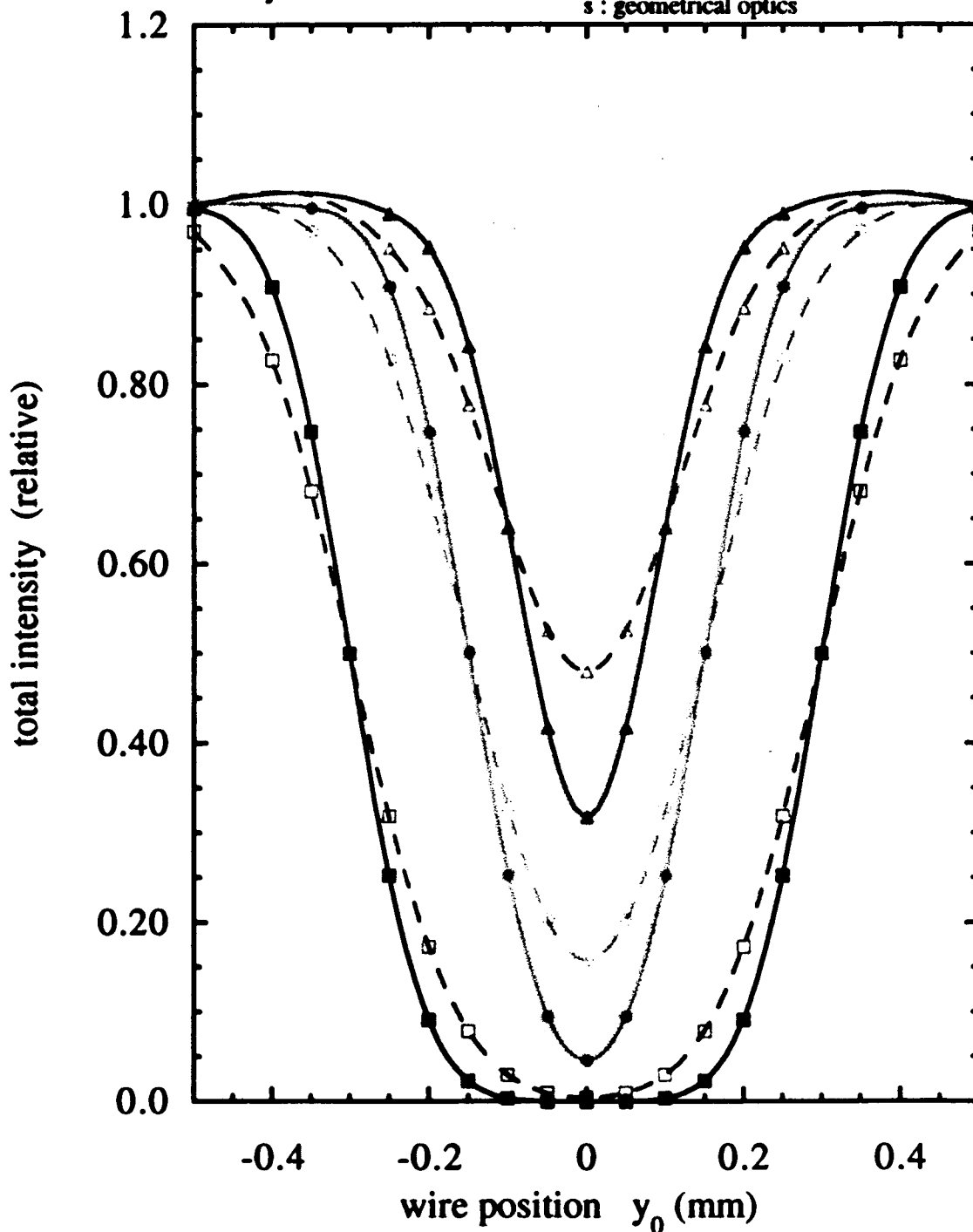
( calc. : wire\_keyence2.nb )



keyence LS5000

d : Fraunhofer diffraction

s : geometrical optics



MacintoshHD:HyperHD:jlc:xtube:ihi:wire\_keyence\_diff1.d

[2] ongoing test of the apparatus

- (i) confirm the performance of current apparatus
- (ii) improve for RDDS construction

(2-1) wire tensioner and cramp

applicable tension  $\leq 9.5$  kgf (slip)

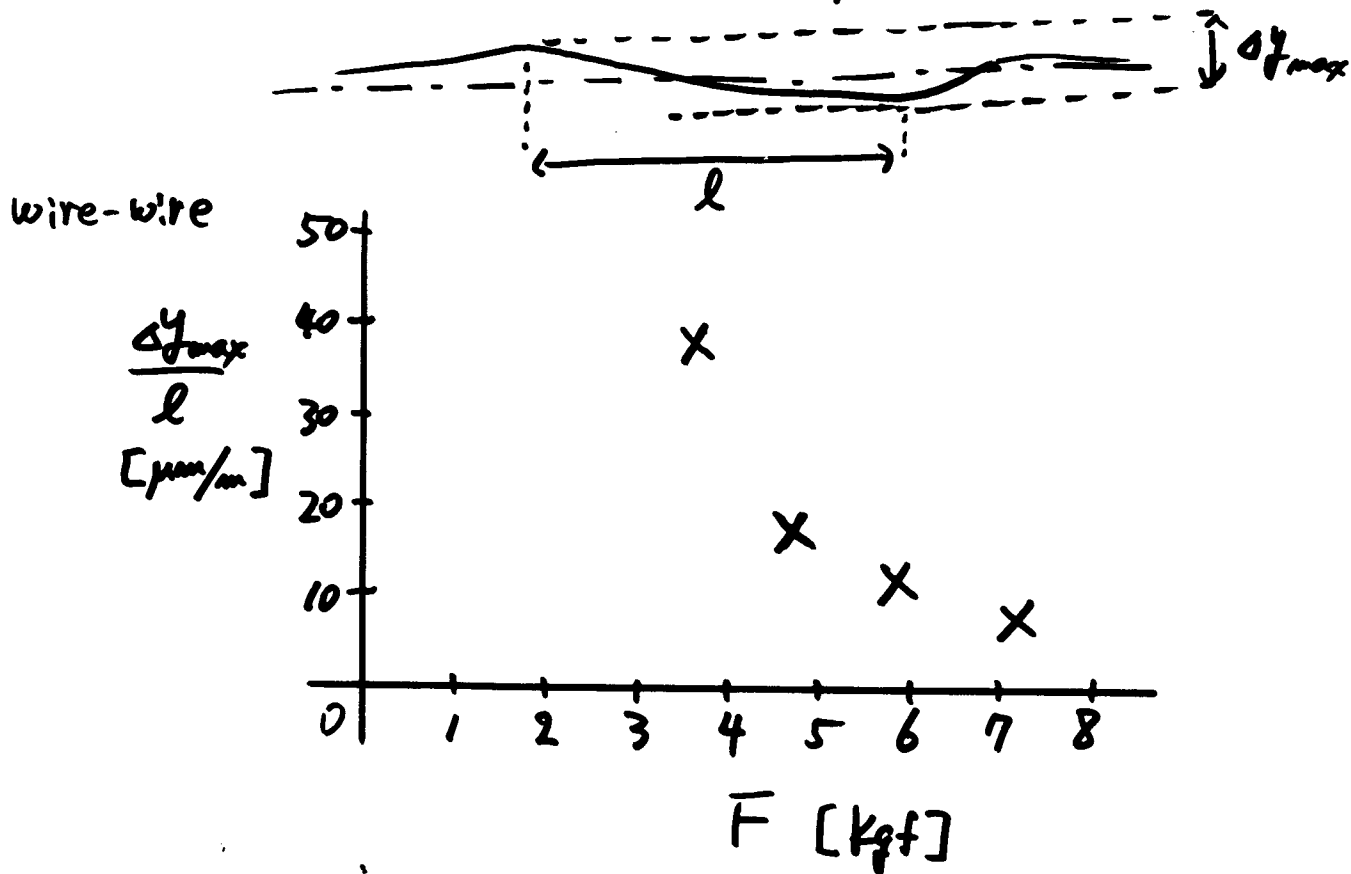
stability  $\frac{\delta F}{F} \approx -1.0 \sim -1.4\% / 5.3$  hours

in  $F = 7.3$  kgf

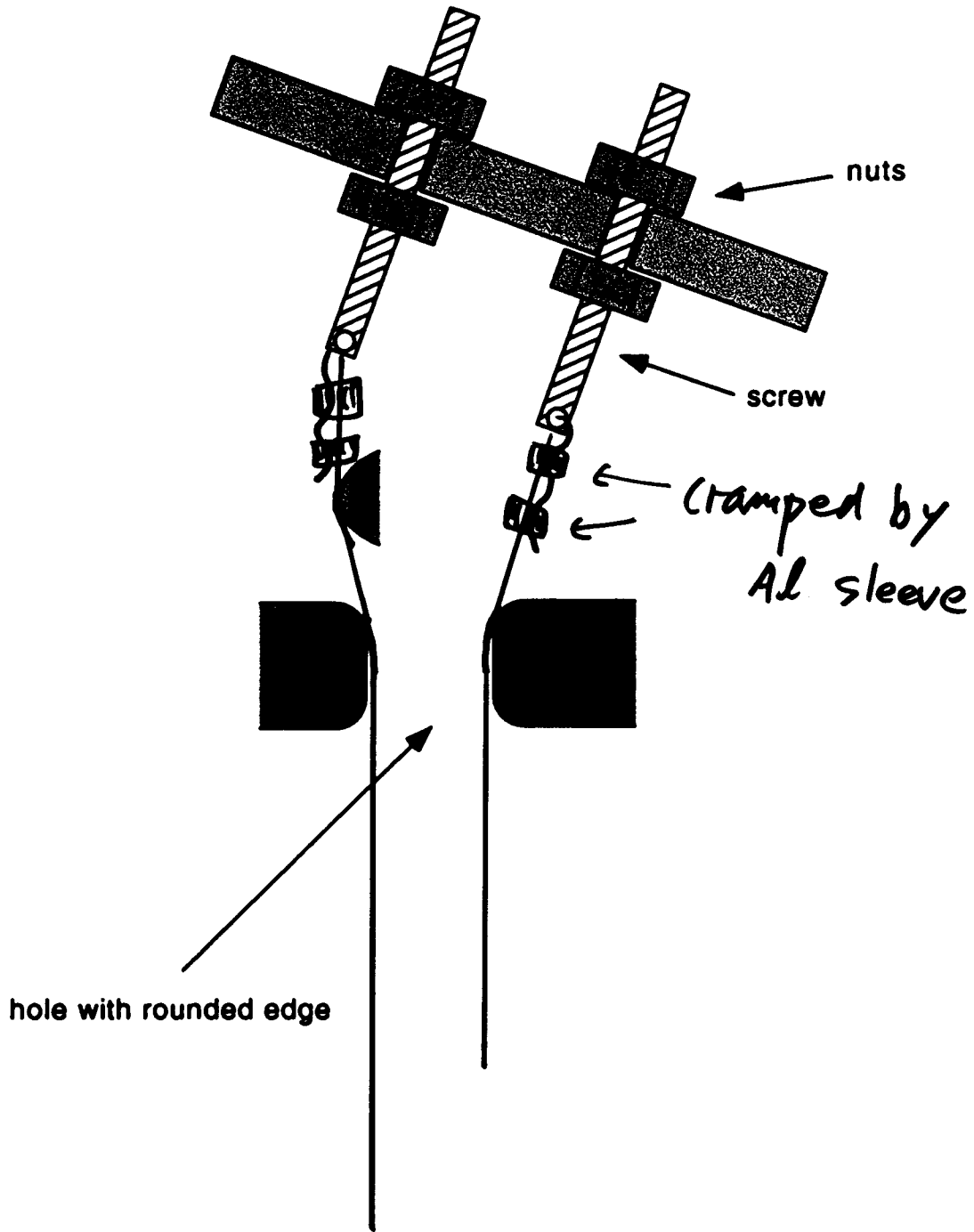
( $\sigma = 1.6$  Pa)

increase friction of cramp  $\rightarrow$  larger tension

(2-2) tension vs lateral deflection



# Wire tensioner and clamp

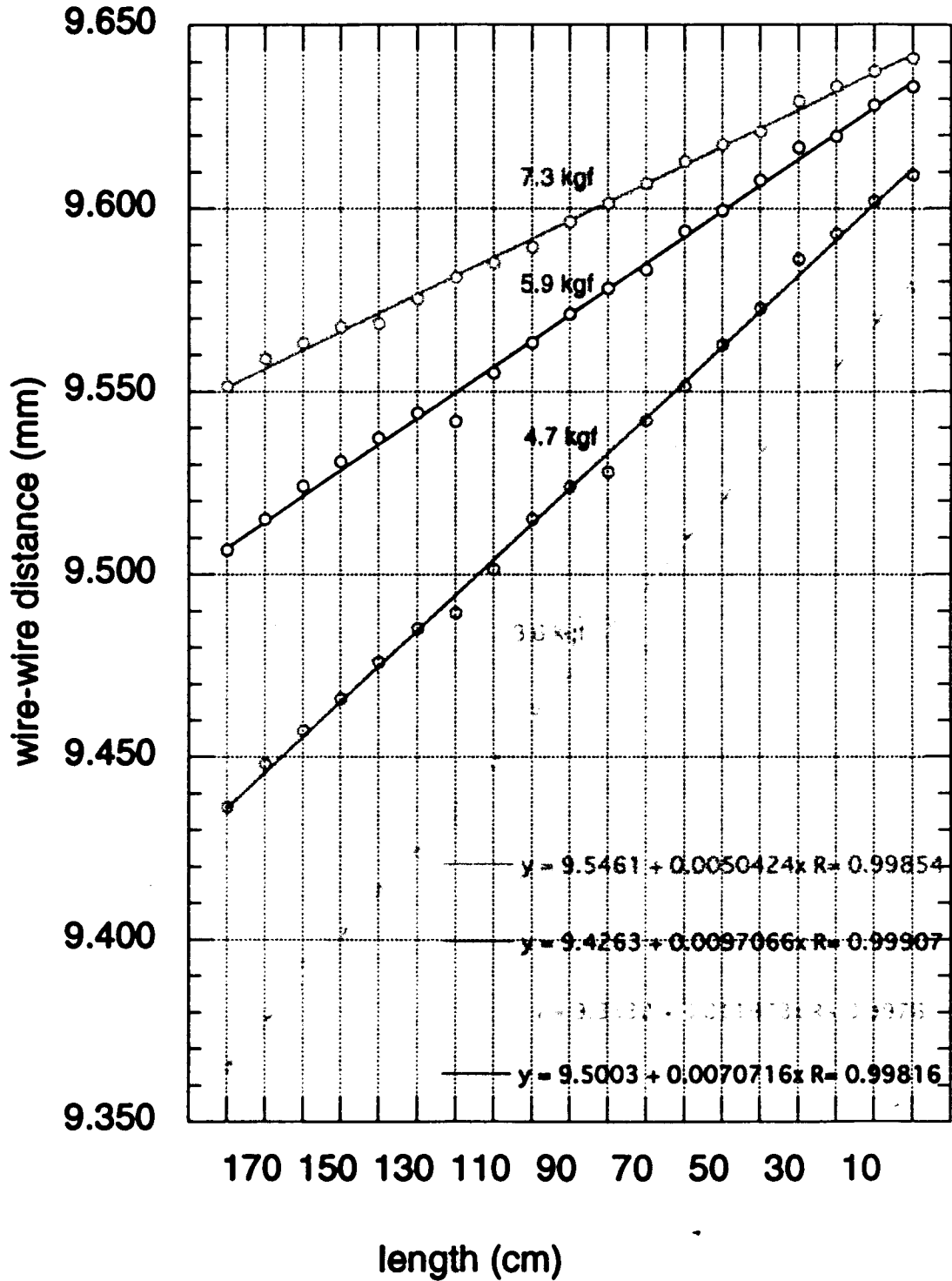




- ch3A (70Hz)
- ch3C (80Hz)
- ch3D (90Hz)
- ch3E (100Hz)

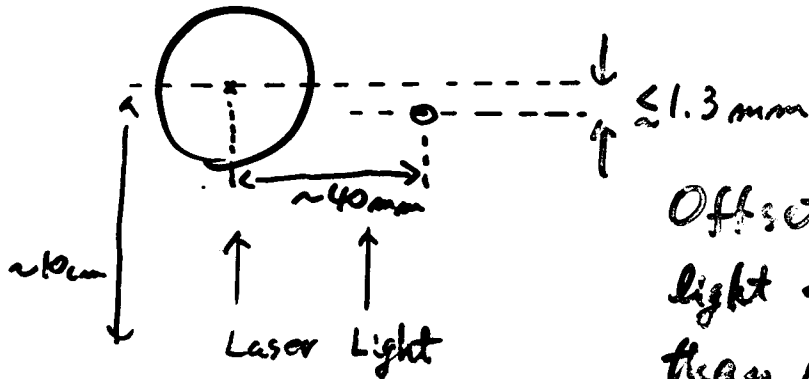
# wire-wire distance in different tension

scan direc.:downward  
average:768



wi0119\_ch3.kgd

(2-3) Effect of torsional motion of stage structure - wire (center-center)  $\sim 40\text{mm}$



Offset along the Laser light should be smaller than 1.3mm.

(1mm deflection  $\rightarrow$   $< 5\mu\text{m}$  read out)

(2-4) averaging

simple moving average

read out  $\{y(t_i)\}$

$$y_{av}(t_n) = \frac{1}{N} \sum_j^N y(t_n - j)$$

random noise  $\sigma_{av} = \frac{\sigma_f}{\sqrt{N}}$

(2-5) move/stop : transient response

Response looked faster than 10ms.

Delay effect was observed when averaging used.

Further test items

(F-1) Selection of better wire material.

(F-2) Wire deformation near edge.

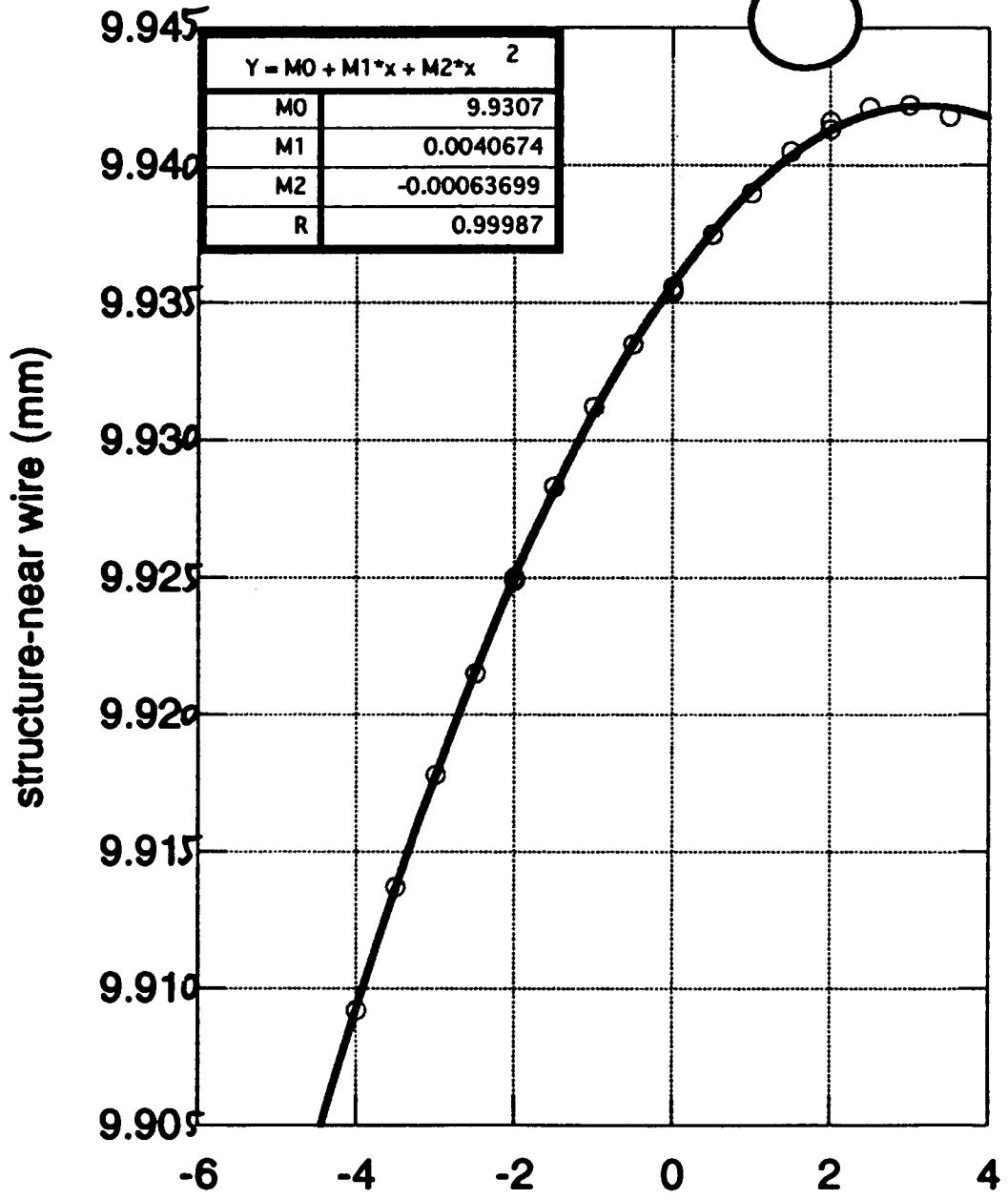
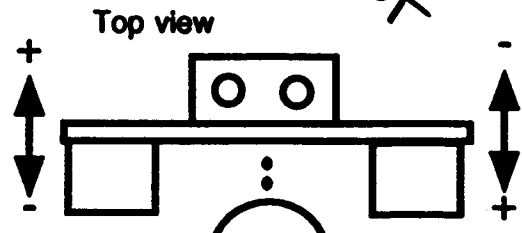
(F-3) Linearity in dynamic range of L.S.M.

MICRO

19 Jan. 1999

# Effect of torsional movement of Laser Scanning Meter

z = 0.9 m  
average = 768  
deform. was measured by dial gauge

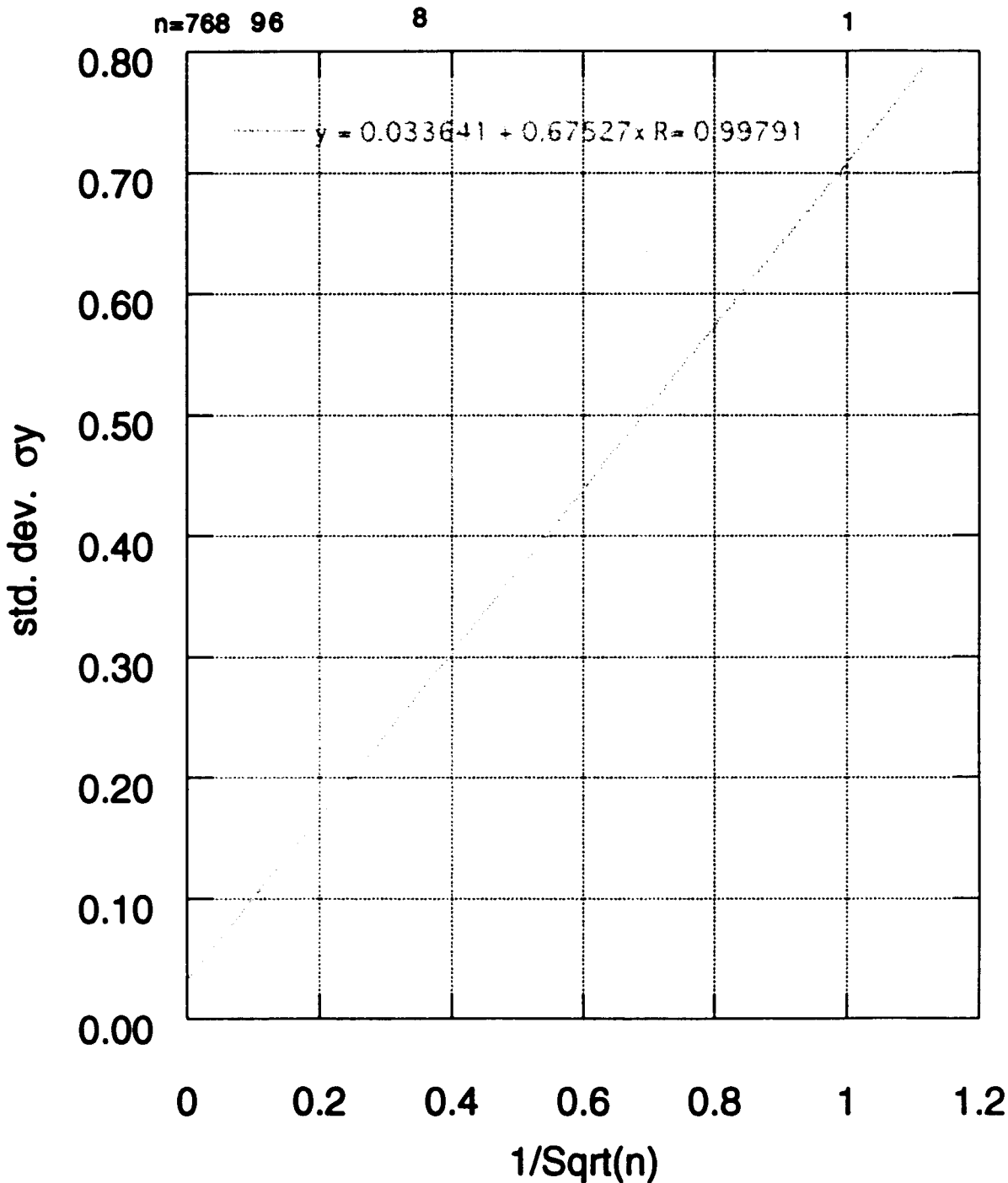


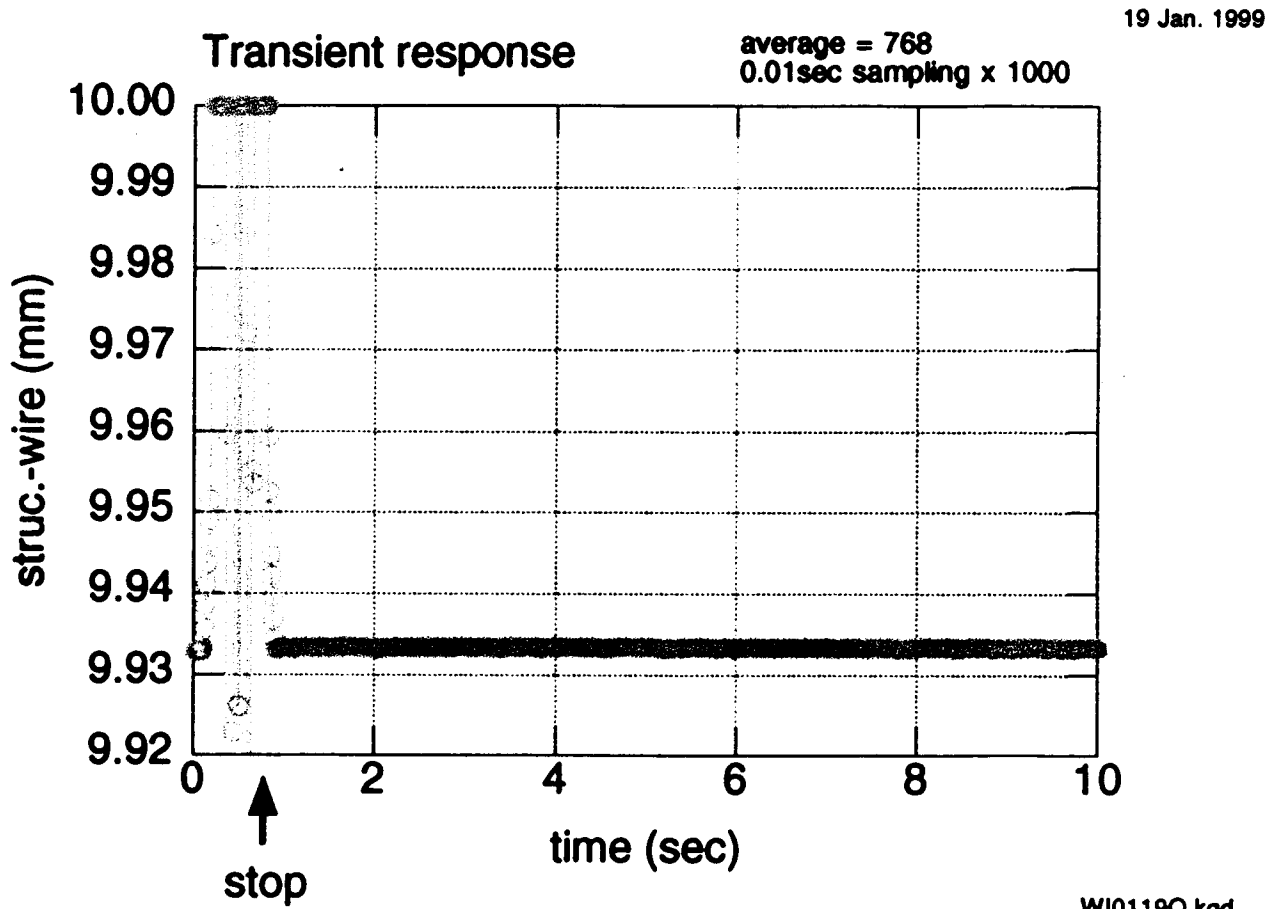
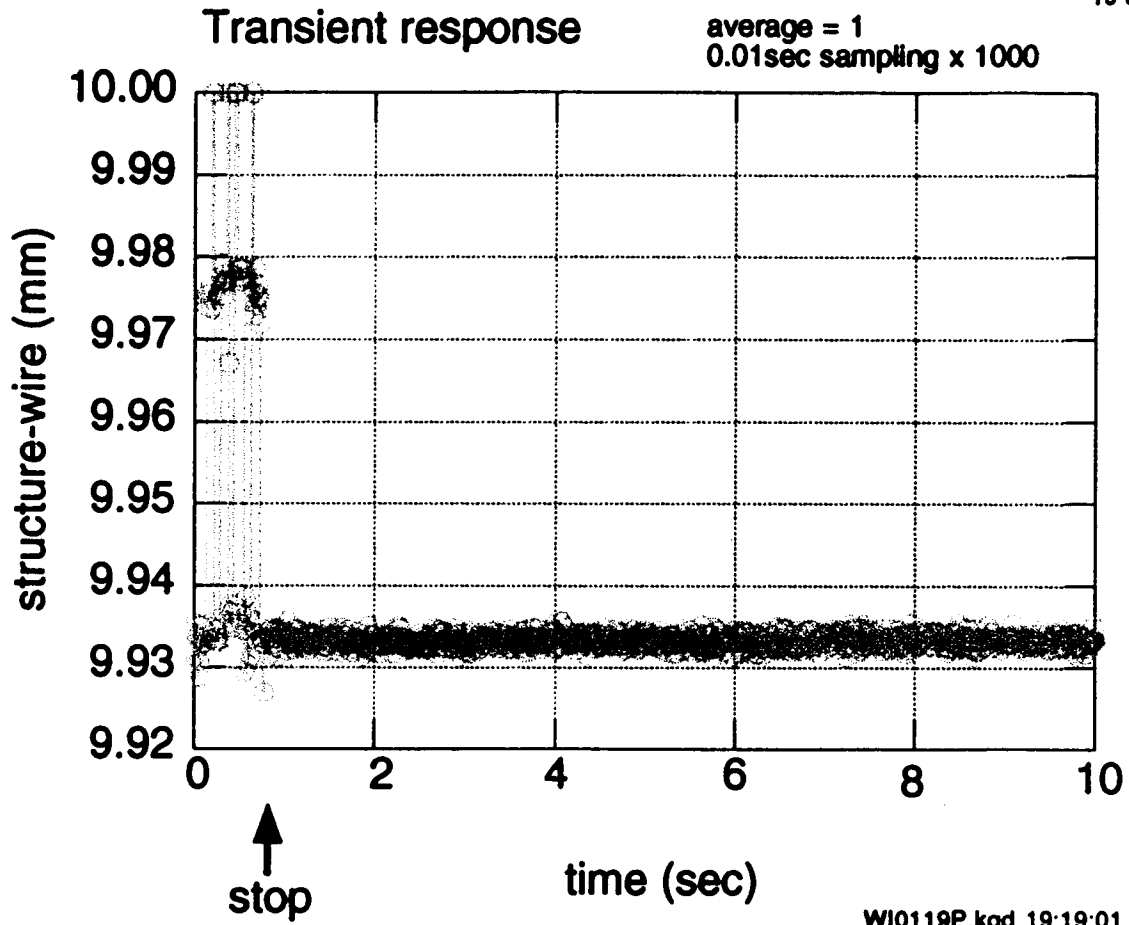
wi0119g.kgd

# Resolution.vs.Averaging.plot

—○— std dev

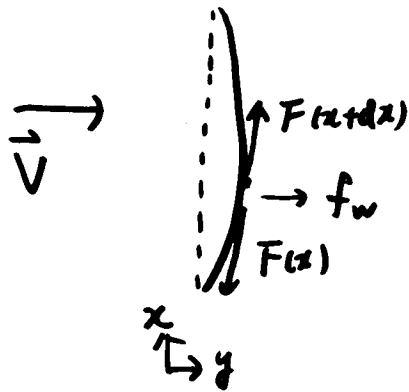
v-wire  $\phi$ 0.3 piano  
Keyence Laser scanning meter  
1sec sampling x 60  
simple moving average





(F-4) Vibration of floor, acoustic noise.

(F-5) Wind



$l$ : length

$F$ : tension

$f_w$ : drag force of wind

$$\left| \frac{dy}{dx} \right| \ll 1 \Rightarrow F \frac{d^2 y}{dx^2} = \frac{f_w}{l}$$

$$\therefore y(x) = \frac{f_w}{2Fl} \left( x - \frac{l}{2} \right) \left( x + \frac{l}{2} \right)$$

max. deflection

$$\left| y \right|_{\max} = \frac{f_w l}{8F}$$

$$(\text{Drag force}) = \frac{1}{2} \rho v^2 A C_0$$

$C_0$ : drag coefficient

$\rho$ : density of fluid

$v$ : fluid velocity

$A$ : projected area of the wire

$$l = 2 \text{ m}, d = 0.3 \text{ mm} \Rightarrow A = 6.0 \times 10^{-4} \text{ m}^2$$

$$F = 7.3 \text{ kgf} = 72 \text{ N}$$

Title

LC-

Name

Date

12/16

Drag coefficient of cylinder  $C_D$

$Re < 0.5 \quad C_D = \frac{8\pi}{Re \cdot (2.002 - \log Re)} \quad (\text{Lamb})$

$5 \leq Re \leq 40 \quad C_D = \left( 0.707 + 3.42 \frac{1}{\sqrt{Re}} \right)^2 \quad (\text{Imai})$

$2 \times 10^4 \leq Re \leq 2 \times 10^5 \quad C_D = 1.2 \quad : \text{constant}$

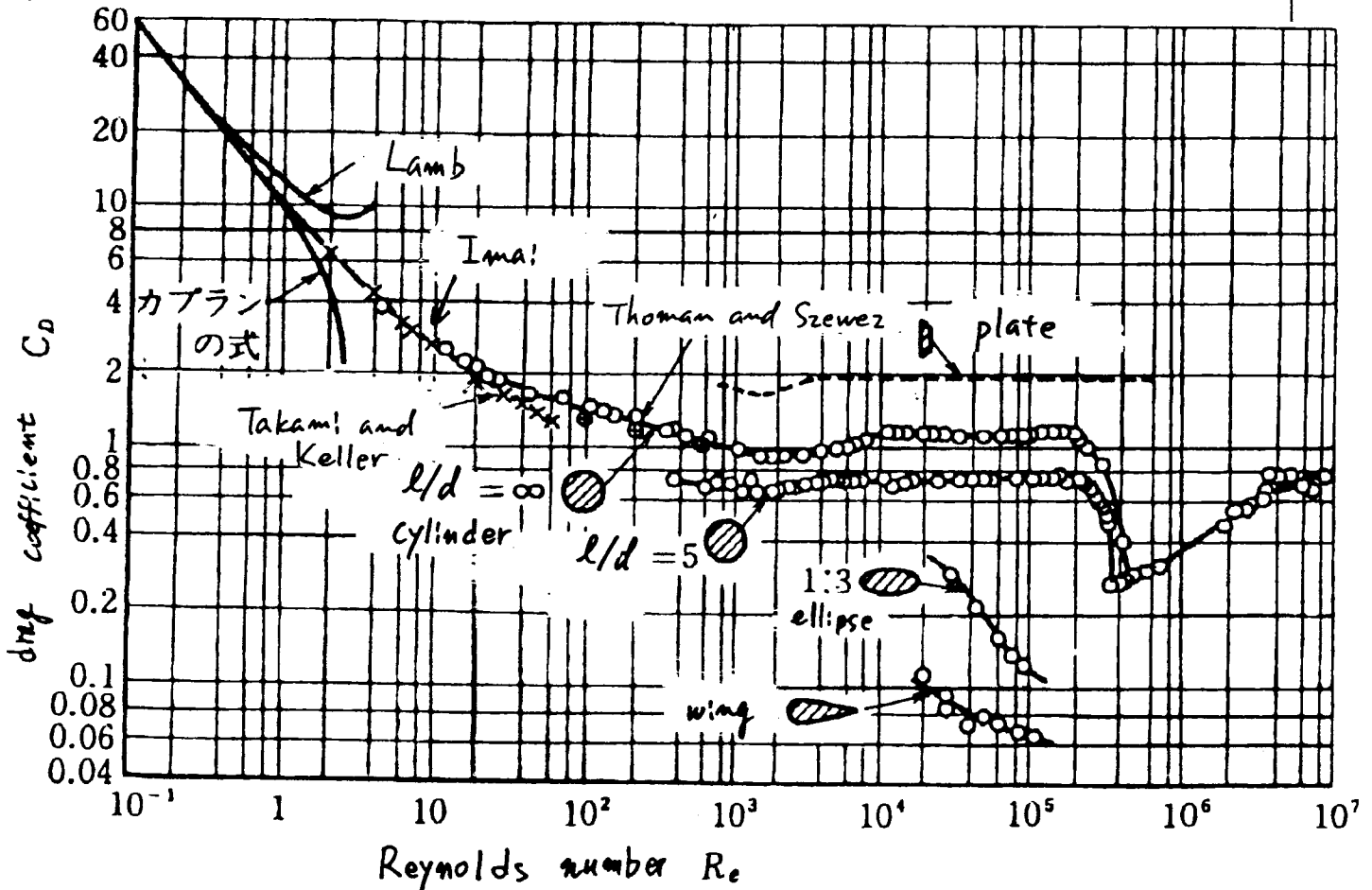
ex.) wire  $\phi 0.3 \text{ mm}, L = 2 \text{ m}$

air 1 atm 25°C dry

$\rho = 1.194 \text{ [kg/m}^3\text{]}$

$\mu = 1.820 \times 10^{-5} \text{ [Pa}\cdot\text{s]}$

$Re = \frac{\rho V d}{\mu} = 19.5 \times \left( \frac{V}{1 \text{ m/s}} \right) \times \left( \frac{d}{0.3 \text{ mm}} \right)$



$$\begin{aligned}\therefore f_w &= \frac{1}{2} \rho V^2 A C_D = \frac{1}{2} \times 1.181 \times 1^2 \times 6.0 \times 10^{-4} \times 2 \\ &= 7.1 \times 10^{-4} \text{ N} \quad \left( \text{air, } v = 1 \text{ m/s} \right. \\ &\quad \left. \phi = 0.3 \text{ mm, } l = 2 \text{ m} \right)\end{aligned}$$

$$\begin{aligned}\therefore |y|_{\max} &= \frac{f_w l}{8 F} \\ &= \frac{7.1 \times 10^{-4} \times 2}{8 \times 72} = 3 \times 10^{-6} \text{ m} \quad \underline{\underline{\quad}}\end{aligned}$$

Vibration induced by Kármán vortex?